

Q2) MOIST AIR AT 60 F DB AND 20% RELATIVE HUMIDITY ENTERS A HEATER AND HUMIDIFIER AT THE RATE OF 2000

Q2) MOIST AIR AT 60 F DB AND 20% RELATIVE HUMIDITY ENTERS A HEATER AND HUMIDIFIER AT THE RATE OF 2000

THE SCENARIO INVOLVING MOIST AIR AT A DRY-BULB TEMPERATURE OF 60°F AND A RELATIVE HUMIDITY OF 20%, ENTERING A COMBINED HEATER AND HUMIDIFIER SYSTEM AT A FLOW RATE OF 2000 UNITS (ASSUMED TO BE IN CUBIC FEET PER MINUTE OR SIMILAR VOLUMETRIC MEASURE), PRESENTS A COMPLEX THERMODYNAMIC PROBLEM. ANALYZING THIS PROCESS REQUIRES UNDERSTANDING THE INITIAL CONDITIONS OF THE AIR, THE BEHAVIOR OF THE AIR AS IT PASSES THROUGH THE HEATING AND HUMIDIFYING EQUIPMENT, AND THE RESULTANT CHANGES IN ITS TEMPERATURE AND MOISTURE CONTENT. THIS COMPREHENSIVE EXPLORATION WILL DELVE INTO THE PROPERTIES OF THE INCOMING MOIST AIR, THE PROCESS OF HEATING AND HUMIDIFICATION, AND THE CALCULATIONS INVOLVED IN DETERMINING THE FINAL STATE OF THE AIR, EMPHASIZING KEY CONCEPTS SUCH AS HUMIDITY RATIO, SPECIFIC HUMIDITY, ENTHALPY, AND THE PSYCHROMETRIC PROCESSES INVOLVED.

UNDERSTANDING THE INITIAL CONDITIONS OF THE MOIST AIR

DRY-BULB TEMPERATURE AND RELATIVE HUMIDITY

THE INITIAL AIR CONDITIONS ARE SPECIFIED AS:

- DRY-BULB TEMPERATURE (T_{DB}): 60°F
- RELATIVE HUMIDITY (RH): 20%

THESE PARAMETERS DEFINE THE STATE OF THE MOIST AIR AND ARE ESSENTIAL FOR CALCULATING OTHER PROPERTIES SUCH AS HUMIDITY RATIO, SPECIFIC HUMIDITY, VAPOR PRESSURE, AND ENTHALPY. THE DRY-BULB TEMPERATURE INDICATES THE TEMPERATURE OF THE AIR AS MEASURED BY A STANDARD THERMOMETER, WHILE THE RELATIVE HUMIDITY INDICATES HOW SATURATED THE AIR IS WITH WATER VAPOR AT THAT TEMPERATURE.

CALCULATING THE SATURATION VAPOR PRESSURE AT 60°F

THE SATURATION VAPOR PRESSURE (P_{SAT}) IS A CRITICAL PARAMETER THAT DEPENDS ON TEMPERATURE. USING EMPIRICAL FORMULAS OR PSYCHROMETRIC CHARTS, THE SATURATION VAPOR PRESSURE AT 60°F IS APPROXIMATELY:

- $P_{SAT} \approx 0.256$ PSI (OR APPROXIMATELY 4.4 INCHES OF MERCURY) BASED ON STANDARD STEAM TABLES.

THIS VALUE INDICATES THE MAXIMUM PARTIAL PRESSURE OF WATER VAPOR THE AIR CAN HOLD AT 60°F.

DETERMINING THE ACTUAL VAPOR PRESSURE AND HUMIDITY RATIO

THE ACTUAL VAPOR PRESSURE (P_v) IS GIVEN BY:

$$P_v = RH \times P_{sat} = 0.20 \times 0.256 \text{ psi} \approx 0.0512 \text{ psi}$$

THE HUMIDITY RATIO (ω), ALSO KNOWN AS THE HUMIDITY OR SPECIFIC HUMIDITY, CAN BE CALCULATED USING THE RELATION:

$$\omega = 0.6219 \times (P_v / (P_{\text{atm}} - P_v))$$

ASSUMING ATMOSPHERIC PRESSURE (P_{atm}) IS APPROXIMATELY 14.7 PSI, THEN:

$$\omega = 0.6219 \times (0.0512 / (14.7 - 0.0512)) \approx 0.6219 \times (0.0512 / 14.6488) \approx 0.6219 \times 0.0035 \approx 0.00218 \text{ lb water vapor per lb dry air}$$

THIS HUMIDITY RATIO INDICATES THE WATER VAPOR CONTENT PER POUND OF DRY AIR IN THE INITIAL STATE.

PROCESS OF HEATING AND HUMIDIFICATION IN THE SYSTEM

FUNCTION OF THE HEATER AND HUMIDIFIER

THE COMBINED HEATER AND HUMIDIFIER SERVE TWO PRIMARY FUNCTIONS:

1. INCREASE THE DRY-BULB TEMPERATURE OF THE INCOMING AIR TO THE DESIRED SETPOINT.
2. ADD MOISTURE TO THE AIR, INCREASING ITS HUMIDITY RATIO TO A TARGET LEVEL SUITABLE FOR THE APPLICATION.

THE PROCESS IS TYPICALLY DESIGNED TO BRING THE INCOMING AIR TO A SPECIFIED CONDITION, OFTEN FOR COMFORT CONTROL, INDUSTRIAL PROCESSES, OR ENVIRONMENTAL REGULATION.

EXPECTED CHANGES IN THE AIR PROPERTIES

- TEMPERATURE INCREASES FROM 60°F TO A HIGHER VALUE (DETERMINED BY SYSTEM DESIGN OR PROCESS REQUIREMENTS).
- HUMIDITY RATIO INCREASES FROM THE INITIAL 0.00218 LB/LB DRY AIR TO A HIGHER VALUE, REFLECTING ADDED MOISTURE.
- ENTHALPY OF THE AIR INCREASES DUE TO BOTH HEATING AND HUMIDIFICATION, AFFECTING THE ENERGY CONSUMPTION AND SYSTEM DESIGN.

PSYCHROMETRIC PROCESS EXPLANATION

THE PROCESS CAN BE VISUALIZED ON A PSYCHROMETRIC CHART, WHERE THE INITIAL STATE POINT (AT 60°F AND 20% RH) MOVES ALONG A PROCESS LINE TO THE FINAL CONDITION. THE MOVEMENT INVOLVES:

1. VERTICAL INCREASE IN TEMPERATURE AT CONSTANT HUMIDITY RATIO (IF ONLY HEATING), OR
2. UPWARD AND RIGHTWARD MOVEMENT IF BOTH HEATING AND HUMIDIFICATION OCCUR SIMULTANEOUSLY.

THE ACTUAL PATH DEPENDS ON THE SYSTEM'S DESIGN—WHETHER IT PRIMARILY HEATS THE AIR, HUMIDIFIES IT, OR DOES BOTH IN TANDEM.

CALCULATIONS FOR FINAL CONDITIONS

DETERMINING THE FINAL HUMIDITY RATIO

THE TARGET HUMIDITY RATIO AFTER HUMIDIFICATION DEPENDS ON SYSTEM SPECIFICATIONS, SUCH AS DESIRED RELATIVE HUMIDITY OR ABSOLUTE HUMIDITY LEVELS. FOR ILLUSTRATION, SUPPOSE THE SYSTEM AIMS TO INCREASE THE HUMIDITY RATIO TO 0.008 LB/LB DRY AIR.

FINAL ENTHALPY CALCULATION

THE SPECIFIC ENTHALPY OF MOIST AIR IS CALCULATED AS:

$$h = 0.24 \times T_{db} + \omega \times (2501 + 1.86 \times T_{db})$$

WHERE:

- h = SPECIFIC ENTHALPY (BTU/LB DRY AIR)
- T_{db} = DRY-BULB TEMPERATURE IN °F
- ω = HUMIDITY RATIO IN LB WATER VAPOR/LB DRY AIR

APPLYING THIS, THE INITIAL ENTHALPY (AT 60°F AND $\omega = 0.00218$) IS:

$$h_{initial} = 0.24 \times 60 + 0.00218 \times (2501 + 1.86 \times 60) \approx 14.4 + 0.00218 \times (2501 + 111.6) \approx 14.4 + 0.00218 \times 2612.6 \approx 14.4 + 5.7 \approx 20.1 \text{ Btu/lb dry air}$$

THE FINAL ENTHALPY DEPENDS ON THE FINAL TEMPERATURE AND HUMIDITY RATIO, WHICH CAN BE DETERMINED BASED ON SYSTEM GOALS.

MASS AND ENERGY BALANCES

GIVEN THE FLOW RATE OF 2000 UNITS (ASSUMED TO BE IN CUBIC FEET PER MINUTE), THE MASS FLOW RATE OF DRY AIR (m_{da}) CAN BE ESTIMATED IF THE AIR DENSITY IS KNOWN. FOR STANDARD CONDITIONS, THE DENSITY OF DRY AIR AT SEA LEVEL IS APPROXIMATELY 0.075 LB/FT³.

$$m_{da} = \text{volumetric flow rate} \times \text{density} = 2000 \text{ ft}^3/\text{min} \times 0.075 \text{ lb/ft}^3 = 150 \text{ lb dry air/min}$$

USING THIS, THE TOTAL MOISTURE ADDED PER MINUTE CAN BE CALCULATED FROM THE CHANGE IN HUMIDITY RATIO:

$$\text{Moisture added} = m_{da} \times (\omega_{final} - \omega_{initial})$$

IMPLICATIONS FOR SYSTEM DESIGN AND OPERATION

ENERGY CONSIDERATIONS

- THE SYSTEM MUST SUPPLY SUFFICIENT HEAT TO RAISE THE AIR TEMPERATURE TO THE DESIRED LEVEL.
- ADDITIONAL ENERGY IS REQUIRED TO HUMIDIFY THE AIR, ESPECIALLY IF THE INITIAL HUMIDITY RATIO IS LOW.
- EFFICIENCY CONSIDERATIONS INCLUDE THE TYPE OF HEATING ELEMENT, HUMIDIFIER TECHNOLOGY, AND HEAT RECOVERY OPTIONS.

CONTROL STRATEGIES

EFFECTIVE CONTROL INVOLVES MONITORING THE INLET CONDITIONS AND ADJUSTING THE HEATER AND HUMIDIFIER OUTPUTS TO MEET THE DESIRED FINAL AIR STATE. THIS MAY INCLUDE:

- USING SENSORS FOR TEMPERATURE AND HUMIDITY.
- EMPLOYING CONTROL ALGORITHMS TO MODULATE HEATING ELEMENTS AND WATER SUPPLY.
- ENSURING STABILITY AND AVOIDING OVERSHOOT OR UNDERSHOOT OF TARGET CONDITIONS.

ENVIRONMENTAL AND COMFORT IMPACTS

PROPERLY CONDITIONED AIR IMPROVES INDOOR AIR QUALITY AND OCCUPANT COMFORT IN HVAC APPLICATIONS. MAINTAINING APPROPRIATE HUMIDITY LEVELS PREVENTS ISSUES SUCH AS DRYNESS, STATIC ELECTRICITY, AND MOLD GROWTH.

CONCLUSION

THE PROCESS INVOLVING MOIST AIR AT 60°F AND 20% RH ENTERING A HEATER AND HUMIDIFIER AT A FLOW RATE OF 2000 UNITS ENCOMPASSES A MULTIFACETED ANALYSIS OF PSYCHROMETRIC PRINCIPLES, ENERGY TRANSFER, AND SYSTEM CONTROL. BY UNDERSTANDING THE INITIAL CONDITIONS

FREQUENTLY ASKED QUESTIONS

WHAT IS THE INITIAL HUMIDITY RATIO OF MOIST AIR AT 60°F DRY BULB TEMPERATURE AND 20% RELATIVE HUMIDITY?

THE INITIAL HUMIDITY RATIO CAN BE CALCULATED USING PSYCHROMETRIC CHARTS OR FORMULAS; AT 60°F AND 20% RH, IT IS APPROXIMATELY 0.0032 LB OF MOISTURE PER LB OF DRY AIR.

HOW DOES PASSING MOIST AIR THROUGH A HEATER AND HUMIDIFIER AT A RATE OF 2000 CFM AFFECT ITS HUMIDITY AND TEMPERATURE?

THE PROCESS INCREASES THE AIR'S TEMPERATURE AND MOISTURE CONTENT, RESULTING IN HIGHER HUMIDITY AND TEMPERATURE, DEPENDING ON THE HEAT AND MOISTURE ADDED BY THE EQUIPMENT.

WHAT IS THE PURPOSE OF A HUMIDIFIER IN THIS AIR TREATMENT PROCESS?

THE HUMIDIFIER ADDS MOISTURE TO THE AIR TO INCREASE ITS HUMIDITY LEVEL, WHICH IS OFTEN NECESSARY FOR COMFORT, PROCESS REQUIREMENTS, OR PREVENTING DRYNESS.

HOW CAN WE DETERMINE THE FINAL CONDITIONS OF THE AIR AFTER HEATING AND HUMIDIFICATION?

BY USING PSYCHROMETRIC CALCULATIONS OR CHARTS, CONSIDERING THE AMOUNT OF HEAT AND MOISTURE ADDED, AND THE INITIAL AIR CONDITIONS, WE CAN DETERMINE THE FINAL TEMPERATURE AND HUMIDITY RATIO.

WHAT FACTORS INFLUENCE THE AMOUNT OF MOISTURE ADDED TO THE AIR DURING THIS PROCESS?

FACTORS INCLUDE THE CAPACITY OF THE HUMIDIFIER, THE DURATION OF CONTACT, THE RATE OF MOISTURE ADDITION (2000 CFM), AND THE INITIAL MOISTURE CONTENT OF THE INCOMING AIR.

WHAT ARE THE TYPICAL APPLICATIONS FOR HEATING AND HUMIDIFYING MOIST AIR IN HVAC SYSTEMS?

COMMON APPLICATIONS INCLUDE MAINTAINING INDOOR AIR QUALITY AND COMFORT, DRYING PROCESSES, STERILIZATION, AND ENSURING PROPER HUMIDITY LEVELS IN MANUFACTURING OR STORAGE ENVIRONMENTS.

ADDITIONAL RESOURCES

MOIST AIR AT 60°F DRY BULB AND 20% RELATIVE HUMIDITY ENTERS A HEATER AND HUMIDIFIER AT THE RATE OF 2000 CFM: AN IN-DEPTH ANALYSIS

INTRODUCTION

IN HVAC (HEATING, VENTILATION, AND AIR CONDITIONING) SYSTEMS, UNDERSTANDING THE BEHAVIOR OF MOIST AIR AS IT PASSES THROUGH VARIOUS HEATING AND HUMIDIFYING PROCESSES IS CRUCIAL FOR MAINTAINING INDOOR AIR QUALITY, COMFORT, AND ENERGY EFFICIENCY. THIS REVIEW FOCUSES ON A SPECIFIC SCENARIO: MOIST AIR AT 60°F DRY BULB TEMPERATURE (DB) AND 20% RELATIVE HUMIDITY (RH) ENTERING A COMBINED HEATER AND HUMIDIFIER AT A FLOW RATE OF 2000 CUBIC FEET PER MINUTE (CFM). WE WILL EXPLORE THE THERMODYNAMIC PRINCIPLES INVOLVED, THE PROPERTIES OF THE INCOMING AIR, THE EFFECTS OF HEATING AND HUMIDIFICATION, AND THE RESULTING CONDITIONS POST-TREATMENT.

1. CHARACTERIZATION OF THE INCOMING AIR

1.1. BASIC PARAMETERS

- DRY BULB TEMPERATURE (DB): 60°F
- RELATIVE HUMIDITY (RH): 20%
- FLOW RATE: 2000 CFM

THE INITIAL STATE OF THE AIR SIGNIFICANTLY INFLUENCES THE ENERGY REQUIREMENTS AND THE HUMIDITY CONTROL STRATEGIES.

1.2. CONVERTING UNITS AND UNDERSTANDING THE CONDITIONS

TO ANALYZE THE AIR, IT IS ESSENTIAL TO CONVERT THE TEMPERATURE AND HUMIDITY INTO MORE USABLE FORMS, SUCH AS HUMIDITY RATIO, SPECIFIC HUMIDITY, AND ENTHALPY.

- TEMPERATURE CONVERSION:

- 60°F IS APPROXIMATELY 15.56°C (USING °F TO °C CONVERSION: $(°F - 32) \times 5/9$).

- SATURATION VAPOR PRESSURE AT 60°F:

- USING STANDARD TABLES, THE SATURATION VAPOR PRESSURE (P_{SAT}) AT 60°F IS APPROXIMATELY 0.256 PSIA (OR ABOUT 1.76 kPa).

- ACTUAL VAPOR PRESSURE (P_v):

- GIVEN RH OF 20%, $P_v = RH \times P_{SAT} = 0.20 \times 0.256 \text{ PSIA} \approx 0.0512 \text{ PSIA}$.

- HUMIDITY RATIO (W):

- THE HUMIDITY RATIO (LB OF MOISTURE PER LB OF DRY AIR) IS GIVEN BY:

$$W = 0.6219 \times \frac{P_v}{P_{ATM} - P_v}$$

- ASSUMING ATMOSPHERIC PRESSURE (P_{ATM}) IS APPROXIMATELY 14.7 PSIA,

$$W = 0.6219 \times \frac{0.0512}{14.7 - 0.0512} \approx 0.6219 \times \frac{0.0512}{14.6488} \approx 0.6219 \times 0.003496 \approx 0.00217 \text{ , LB/LB DRY AIR}$$

- ENTHALPY OF THE INCOMING AIR:

- ENTHALPY (H) OF MOIST AIR CAN BE APPROXIMATED AS:

$$H = 0.24 \times T_{DB} + W \times (2501 + 1.86 \times T_{DB})$$

- SUBSTITUTING THE VALUES:

$$H = 0.24 \times 60 + 0.00217 \times (2501 + 1.86 \times 60)$$

$$H = 14.4 + 0.00217 \times (2501 + 111.6) = 14.4 + 0.00217 \times 2612.6 \approx 14.4 + 5.67 \approx 20.07 \text{ BTU/LB DRY AIR}$$

THIS INITIAL CHARACTERIZATION PROVIDES A BASELINE FOR UNDERSTANDING HOW THE AIR WILL CHANGE AFTER PASSING THROUGH THE HEATER AND HUMIDIFIER.

2. THERMODYNAMIC AND PSYCHROMETRIC PRINCIPLES

2.1. PSYCHROMETRICS OVERVIEW

PSYCHROMETRICS INVOLVES THE STUDY OF THE THERMODYNAMIC PROPERTIES OF MOIST AIR. KEY PARAMETERS INCLUDE:

- DRY BULB TEMPERATURE (T_{DB})

- WET BULB TEMPERATURE (T_{wb})
- HUMIDITY RATIO (W)
- RELATIVE HUMIDITY (RH)
- ENTHALPY (H)

UNDERSTANDING HOW THESE PARAMETERS INTERACT HELPS IN DESIGNING SYSTEMS THAT MODIFY AIR CONDITIONS EFFICIENTLY.

2.2. HEATING AND HUMIDIFICATION PROCESSES

THE SYSTEM INVOLVES TWO SIMULTANEOUS PROCESSES:

- HEATING: RAISING THE DRY BULB TEMPERATURE OF THE AIR.
- HUMIDIFICATION: INCREASING THE MOISTURE CONTENT (HUMIDITY RATIO).

THE PRIMARY GOAL IS TO ACHIEVE DESIRED INDOOR AIR CONDITIONS WHILE OPTIMIZING ENERGY USE.

3. EFFECTS OF HEATING AND HUMIDIFICATION

3.1. HEATING THE AIR

HEATING THE MOIST AIR INVOLVES ADDING SENSIBLE HEAT, WHICH RAISES THE TEMPERATURE WITHOUT CHANGING THE MOISTURE CONTENT (ASSUMING NO MOISTURE IS ADDED OR REMOVED DURING HEATING).

- TEMPERATURE INCREASE:
 - THE FINAL DRY BULB TEMPERATURE DEPENDS ON THE AMOUNT OF HEAT SUPPLIED.
 - THE TEMPERATURE RISE IS CALCULATED BASED ON THE HEAT INPUT AND THE MASS FLOW RATE.
- IMPACT ON RELATIVE HUMIDITY:
 - AS TEMPERATURE INCREASES, THE RELATIVE HUMIDITY TENDS TO DECREASE IF THE MOISTURE CONTENT REMAINS CONSTANT BECAUSE WARMER AIR CAN HOLD MORE MOISTURE.

3.2. HUMIDIFICATION

HUMIDIFICATION ADDS MOISTURE TO THE AIR, INCREASING THE HUMIDITY RATIO.

- METHODS:
 - EVAPORATIVE HUMIDIFIERS ADD MOISTURE DIRECTLY TO THE AIR.
 - THE AMOUNT OF MOISTURE ADDED DEPENDS ON THE SYSTEM DESIGN AND DESIRED FINAL CONDITIONS.
- EFFECT ON PSYCHROMETRIC CHART:
 - MOVING HORIZONTALLY TO THE RIGHT (INCREASING W) AT CONSTANT TEMPERATURE IF MOISTURE IS ADDED AT CONSTANT TEMPERATURE.
 - OR, MOVING ALONG A LINE OF CONSTANT ENTHALPY IF HEAT IS ADDED SIMULTANEOUSLY.

4. CALCULATING THE POST-TREATMENT CONDITIONS

GIVEN THE INITIAL CONDITIONS AND FLOW RATE, WE ANALYZE THE POTENTIAL OUTCOMES AFTER PASSING THROUGH THE HEATER AND HUMIDIFIER.

4.1. MASS FLOW RATE OF DRY AIR

- CONVERSION TO MASS FLOW:

- AT 2000 CFM, THE MASS FLOW RATE (M) OF DRY AIR IS:

$$M = \frac{\text{CFM} \times \text{Density of Air}}{60}$$

- THE DENSITY OF AIR AT APPROXIMATELY 15.56°C (60°F) AND ATMOSPHERIC PRESSURE IS ROUGHLY 0.075 LB/FT³.

$$M = \frac{2000 \times 0.075}{60} = \frac{150}{60} = 2.5 \text{ , LB/SEC}$$

- ALTERNATIVELY, IN LB/MIN:

$$2.5 \times 60 = 150 \text{ , LB/MIN}$$

4.2. MOISTURE ADDITION AND HEATING

SUPPOSE THE SYSTEM AIMS TO:

- RAISE THE AIR TEMPERATURE TO A COMFORTABLE INDOOR CONDITION, SAY 70°F (21.1°C).
- ACHIEVE A SPECIFIC HUMIDITY LEVEL SUITABLE FOR COMFORT, SAY RH OF 40%.

STEP-BY-STEP:

1. DETERMINE THE DESIRED FINAL CONDITIONS:

- FINAL TEMPERATURE: 70°F (~21.1°C)
- TARGET RH: 40%

2. FIND THE SATURATION VAPOR PRESSURE AT 70°F:

- P_{SAT} AT 70°F (~21.1°C): APPROXIMATELY 0.863 PSIA.

3. CALCULATE THE VAPOR PRESSURE FOR 40% RH:

$$P_v = 0.40 \times 0.863 \approx 0.345 \text{ PSIA}$$

4. DETERMINE THE HUMIDITY RATIO AT THESE CONDITIONS:

$$W_{\text{FINAL}} = 0.6219 \times \frac{0.345}{14.7 - 0.345} \approx 0.6219 \times \frac{0.345}{14.355} \approx 0.6219 \times 0.024 \approx 0.0149 \text{ , LB/LB DRY AIR}$$

5. CALCULATE THE MOISTURE TO BE ADDED:

- INITIAL W: 0.00217 LB/LB DRY AIR.
- FINAL W: 0.0149 LB/LB DRY AIR.

- MOISTURE ADDED PER LB OF DRY AIR:

$$W_{\text{FINAL}} - W_{\text{INITIAL}} = 0.0149 - 0.00217 = 0.01273 \text{ , LB/LB DRY AIR}$$

$$\Delta W = 0.0149 - 0.00217 \approx 0.01273 \text{ lb}$$

6. TOTAL MOISTURE ADDED PER MINUTE:

$$150 \text{ lb/min} \times 0.01273 \approx 1.91 \text{ lb/min}$$

7. ENERGY REQUIRED FOR HEATING:

- TO RAISE TEMPERATURE FROM 60°F TO 70°F:

$$\Delta T = 10^\circ \text{F}$$

- SENSIBLE HEAT:

$$Q_{\text{SENSIBLE}} = M \times C_p \times \Delta T$$

- WITH $C_p \approx 0.24 \text{ BTU/lb}^\circ \text{F}$:

$$Q_{\text{SENSIBLE}} = 150 \times 0.24 \times 10 = 360 \text{ BTU/min}$$

8. LATENT HEAT FOR ADDED MOISTURE:

- APPROXIMATE LATENT HEAT

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