

# MT BNH XE BAO GM 1 VNH BNH XE C KHI LNG M=5kg V 8 CM, MI CM C KHI LNG M=1kg V DI R=0,4m, ANG LN TRN MT

MT BNH XE BAO GM 1 VNH BNH XE C KHI LNG M=5kg V 8 CM, MI CM C KHI LNG M=1kg V DI R=0,4m, ANG LN TRN MT

TRONG L<sub>1</sub> NH V<sub>1</sub> C V<sub>1</sub> T L<sub>1</sub> V<sub>1</sub> C<sub>1</sub> H<sub>1</sub> C, C<sub>1</sub> C B<sub>1</sub> I TO<sub>1</sub> N LI<sub>1</sub> N QUAN<sub>1</sub> P<sub>1</sub> N S<sub>1</sub> CHUY<sub>1</sub> N<sub>1</sub> P<sub>1</sub> NG C<sub>1</sub> A C<sub>1</sub> C V<sub>1</sub> M<sub>1</sub> T HO<sub>1</sub> C TRONG M<sub>1</sub> I TR<sub>1</sub> P<sub>1</sub> NG KH<sub>1</sub> NG<sub>1</sub> P<sub>1</sub> NG NH<sub>1</sub> T LU<sub>1</sub> N THU H<sub>1</sub> T S<sub>1</sub> QUAN T<sub>1</sub> M C<sub>1</sub> ANHI<sub>1</sub> UNG<sub>1</sub> P<sub>1</sub> I H<sub>1</sub> C GIA NGHI<sub>1</sub> N C<sub>1</sub> U<sub>1</sub> P<sub>1</sub> C B<sub>1</sub> T, C<sub>1</sub> C B<sub>1</sub> I TO<sub>1</sub> N LI<sub>1</sub> N QUAN<sub>1</sub> P<sub>1</sub> N KH<sub>1</sub> IL<sub>1</sub> P<sub>1</sub> NG, V<sub>1</sub> N T<sub>1</sub> C, G<sub>1</sub> CNGHI<sub>1</sub> NG V<sub>1</sub> C H<sub>1</sub> C NH<sub>1</sub> B<sub>1</sub> N K<sub>1</sub> NH QU<sub>1</sub> P<sub>1</sub> P<sub>1</sub> O MANG L<sub>1</sub> INHI<sub>1</sub> U TH<sub>1</sub> TH<sub>1</sub> CH V<sub>1</sub> C<sub>1</sub> H<sub>1</sub> I<sub>1</sub> P<sub>1</sub> HI<sub>1</sub> UR<sub>1</sub> H<sub>1</sub> N V<sub>1</sub> C<sub>1</sub> CNG L<sub>1</sub> C V<sub>1</sub> CHUY<sub>1</sub> N<sub>1</sub> P<sub>1</sub> NG. TRONG B<sub>1</sub> I VI<sub>1</sub> T N<sub>1</sub> Y, CH<sub>1</sub> NG TA S<sub>1</sub> P<sub>1</sub> IS<sub>1</sub> U V<sub>1</sub> O PH<sub>1</sub> N T<sub>1</sub> CH<sub>1</sub> BNH XE I TO<sub>1</sub> N C<sub>1</sub> BAO GM 1 VNH BNH XE C KHI LNG M=5kg V 8 CM, MI CM C KHI LNG M=1kg V DI R=0,4m, ANG LN TRN MT. C<sub>1</sub> C Y<sub>1</sub> U T<sub>1</sub> NH<sub>1</sub> KH<sub>1</sub> IL<sub>1</sub> P<sub>1</sub> NG XE, K<sub>1</sub> CH TH<sub>1</sub> P<sub>1</sub> C, G<sub>1</sub> CNGHI<sub>1</sub> NG, V<sub>1</sub> N T<sub>1</sub> C, V<sub>1</sub> QU<sub>1</sub> P<sub>1</sub> P<sub>1</sub> O S<sub>1</sub> P<sub>1</sub> P<sub>1</sub> C PH<sub>1</sub> N T<sub>1</sub> CH K<sub>1</sub> HI<sub>1</sub> UR<sub>1</sub> H<sub>1</sub> N V<sub>1</sub> QU<sub>1</sub> TR<sub>1</sub> NH CHUY<sub>1</sub> N<sub>1</sub> P<sub>1</sub> NG C<sub>1</sub> A C<sub>1</sub> C V<sub>1</sub> T TH<sub>1</sub> TRONG C<sub>1</sub> C<sub>1</sub> I<sub>1</sub> U KI<sub>1</sub> N N<sub>1</sub> Y.

PH<sub>1</sub> N T<sub>1</sub> CH C<sub>1</sub> C Y<sub>1</sub> U T<sub>1</sub> C<sub>1</sub> A B<sub>1</sub> I TO<sub>1</sub> N

## 1. TH<sub>1</sub> NG S<sub>1</sub> C<sub>1</sub> A C<sub>1</sub> C V<sub>1</sub> T TH<sub>1</sub>

- KH<sub>1</sub> IL<sub>1</sub> P<sub>1</sub> NG C<sub>1</sub> MA XE
- CHI<sub>1</sub> U D<sub>1</sub> I C<sub>1</sub> A XE
- KH<sub>1</sub> IL<sub>1</sub> P<sub>1</sub> NG TH<sub>1</sub> MI HAI
- CHI<sub>1</sub> U D<sub>1</sub> I C<sub>1</sub> A KH<sub>1</sub> IL<sub>1</sub> P<sub>1</sub> NG TH<sub>1</sub> HAI: C X<sub>1</sub> C<sub>1</sub> P<sub>1</sub> NH R<sub>1</sub> H<sub>1</sub> N TRONG QU<sub>1</sub> TR<sub>1</sub> NH PH<sub>1</sub> N T<sub>1</sub> CH)
- V<sub>1</sub> N T<sub>1</sub> C C<sub>1</sub> A V<sub>1</sub> D R=0,4m
- G<sub>1</sub> CNGHI<sub>1</sub> NG C<sub>1</sub> A M<sub>1</sub> T PH<sub>1</sub> NG LN TRN MT

C<sub>1</sub> C TH<sub>1</sub> NG S<sub>1</sub> N<sub>1</sub> Y<sub>1</sub> P<sub>1</sub> NG VAI TR<sub>1</sub> QUAN TR<sub>1</sub> NG TRONG VI<sub>1</sub> C X<sub>1</sub> C<sub>1</sub> P<sub>1</sub> NH C<sub>1</sub> C L<sub>1</sub> C T<sub>1</sub> C D<sub>1</sub> NG, N<sub>1</sub> NG L<sub>1</sub> QU<sub>1</sub> P<sub>1</sub> P<sub>1</sub> O CHUY<sub>1</sub> N<sub>1</sub> P<sub>1</sub> NG C<sub>1</sub> A C<sub>1</sub> C V<sub>1</sub> T TH<sub>1</sub> TRONG H<sub>1</sub> TH<sub>1</sub> NG.

HI<sub>1</sub> UR<sub>1</sub> V<sub>1</sub> CHUY<sub>1</sub> N<sub>1</sub> P<sub>1</sub> NG C<sub>1</sub> A XE TR<sub>1</sub> N M<sub>1</sub> T PH<sub>1</sub> NG NGHI<sub>1</sub> NG

## 1. C<sub>1</sub> C L<sub>1</sub> C T<sub>1</sub> C D<sub>1</sub> NG L<sub>1</sub> N XE

TRONG QU<sub>1</sub> TR<sub>1</sub> NH CHUY<sub>1</sub> N<sub>1</sub> P<sub>1</sub> NG C<sub>1</sub> A XE TR<sub>1</sub> N M<sub>1</sub> T PH<sub>1</sub> NG NGHI<sub>1</sub> NG, C<sub>1</sub> C L<sub>1</sub> C SAU<sub>1</sub> P<sub>1</sub> Y<sub>1</sub> P<sub>1</sub> NG VAI TR<sub>1</sub>

- TR<sub>1</sub> NG L<sub>1</sub> C (G)=M G, TRONG P<sub>1</sub> P<sub>1</sub> G ≈ 9,8 m/s<sup>2</sup>
- L<sub>1</sub> C PH<sub>1</sub> N L<sub>1</sub> C (ND): N<sub>1</sub> NG C<sub>1</sub> A M<sub>1</sub> T PH<sub>1</sub> NG L<sub>1</sub> N XE
- L<sub>1</sub> C MA S<sub>1</sub> T (F)<sub>1</sub> THU<sub>1</sub> C V<sub>1</sub> O<sub>1</sub> P<sub>1</sub> C<sub>1</sub> I<sub>1</sub> M C<sub>1</sub> A M<sub>1</sub> T PH<sub>1</sub> NG V<sub>1</sub> V<sub>1</sub> T LI<sub>1</sub> U
- L<sub>1</sub> C K<sub>1</sub> O HO<sub>1</sub> C<sub>1</sub> P<sub>1</sub> Y (N)<sub>1</sub> U C<sub>1</sub> H<sub>1</sub> O<sub>1</sub> I<sub>1</sub> U KI<sub>1</sub> N B<sub>1</sub> I TO<sub>1</sub> N C<sub>1</sub> TH<sub>1</sub>

TRONG NHỊP U BỊ I TO N, L C TR NG TR Ị NG PH N TH NH HAI TH NH PH N: TH NH PH N VU NG G C V I M TH NH PH N SONG SONG V I M T PH NG, Ị NH H Ị NG TR C TI P Ị Ị N QU TR NH CHUY N Ị Ị NG.

2. PH N T CH C C TH NH PH N L C

- TH NH PH N C A TR NG L C SONG SONG V I M G T PH N NG(Θ)
- TH NH PH N C A TR NG L C VU NG G C M N T PH N NG(Θ)

TRONG Ị Ị , Θ L G C NGHI NG C A M T PH NG. C C TH NH PH N N Y QUY T Ị Ị NH Ị Ị L N C A L DI CHUY N C A V T TH .

PH Ị NG PH P GI I B I TO N CHUY N Ị Ị NG

1. S D NG Ị NH LU T NEWTON

Ị PH N T CH CHUY N Ị Ị NG, TA Ị P D NG Ị NH LU T II NEWTON:

•  $F = m a$

TRONG Ị Ị , F L T NG C C L C T C D NG L N V T TH THEO PH Ị NG CHUY N Ị Ị NG, V A L GIA T

2. T NH TO N GIA T C C A XE

D A V O L C T C D NG, TA C :

•  $GIA\ T\ C\ A = (F\_T\ NG) / m$

TRONG Ị Ị , F\_T NG C TH L TH NH PH N C A TR NG L C TR Ị C C L C C N NH MA S T.

3. T NH V N T C CU I C NG

N U BỊ T V N T C BAN Ị Ị U (V<sub>0</sub>) V GIA T C (A), V N T C SAU M T TH I GIAN T HO C SAU QU NG Ị Ị T NH B NG C NG TH C:

- $V = v_0 + a t$
- Ho C THEO C NG TH C CHUY N Ị Ị NG TH NG BI N Ị Ị I Ị U:  $R = v_0 t + (1/2) a t^2$

PH N T CH QU Ị Ị O V G C NGHI NG

## 1. T P C P P NG C P A G P C NGHI P NG P P N CHUY P N P P NG

G P C NGHI P NG P NH H P P NG P P N TH P NH PH P N L P C SONG SONG C P A TR P NG L P C, T P P P QUY P T P P NH GI XE DI CHUY P N HO P C TR P P T XU P NG M P T PH P NG.

## 2. QU P P P O C P A V P T TH P

TRONG TR P P NG H P P C P C V P T TH P CHUY P N P P NG THEO QU P P P O, NH P KH P I L P P NG MI DI R = 0,4M V QU P P P O S P L P M P T P O P N P P P NG CONG HO P C TH P NG T P Y THU P C V P O L P C T P C D P NG V P P I P

## P NG D P NG C P A B P I TO P N TRONG TH P C T P

### 1. THI P T K P H P TH P NG V P N CHUY P N

C P C K P S P C P TH P D P A V P O PH P N T P CH N P Y P P THI P T K P C P C H P TH P NG V P N CHUY P N NH P THAN HO P C P P P NG RAY NGHI P NG P P T P I P U H P A HI P U QU P V P AN TO P N.

### 2. P P O T P O K P N P NG GI P I B P I T P P V P T L P

C P C SINH VI P N V P NH P NGHI P N C P U C P TH P P P D P NG PH P P NG PH P P PH P N T P CH L P C, GIA T P C, V P QU P B P I TO P N T P P NG T P , N P NG CAO K P N P NG V P KI P N TH P C CHUY P N M P N.

## CH P P KHI GI P I C P C B P I TO P N CHUY P N P P NG

- CH P P P P N C P C Y P U T P NH P MA S P T, L P C C P N, V P P I P U KI P N BAN P P U C P A V P T TH P .
- PH P N T P CH R P C P C TH P NH PH P N L P C THEO PH P P NG VU P NG G P C V P SONG SONG V P I M P T PH P NG.
- S P D P NG P P NG C P C C P NG TH P C V P T L P LI P N QUAN P P N CHUY P N P P NG P P U, BI P N P P I P P
- P P T T P N BI P N R P R P NG P P D P THEO D P I C P C B P P C T P NH TO P N.

## K P T LU P N

TRONG B P I VI P T N P Y, CH P NG TA P P PH P N T P CH M B N H X E B A O G m 1 V n h B N H X E C K H I L n g M = 5 k g V 8 C m , M i C m C K H I L n g M = 1 k g V D i R = 0 , 4 m , A n g L n T r n M t , C P N G C P C Y P U T P L I P N Q U A N N H P K H P I L P P N G , C H I P U V P N T P C , G P C N G H I P N G V P Q U P P P O C H U Y P N P P N G . H i P U R P C P C N G U Y P N L P C P B P N V P C P C H P V P T L P S P G I P P B P N G I P I Q U Y P T C P C B P I T O P N T P P N G T P M P T C P C H C H P N H X P C V P H I P U Q U P . N K H P N G C H P H P U P C H T R O N G H P C T P P M P C P N C P P N G D P N G T H P C T P T R O N G T H I P T K P H P T H P N G V P N C V P C P C L P N H V P C L I P N Q U A N P P N C P H P C C H U Y P N P P N G .

H Y V P N G B P I V I P T P P C U N G C P P C H O B P N C P I N H P N T O P N D I P N V P M P T B P I T O P N C H U Y P N P P N G P H P G I P P B P N N P N G C A O K P N P N G P H P N T P C H V P G I P I Q U Y P T C P C V P N P P V P T L P T R O N G T H P C T P .

## FREQUENTLY ASKED QUESTIONS

C[?] CH T[?] NH V[?] N T[?] C C[?] A XE B[?] NH XE KHI CHUY[?] N [?] [?] NG TRONG B[?] I TO[?] M  
G[?] ?

V[?] NT[?] C C[?] A XE B[?] NH XE [?] [?] [?] C T[?] NH D[?] A TR[?] NM[?] I LI[?] NH[?] GI[?] A V[?] NT[?] C C[?] A TR[?] C B[?] NH XE V[?]  
XE, THEO C[?] NG TH[?] C V = R  $\Omega$ , TRONG [?] [?]  $\Omega$  L[?] T[?] C[?] [?] G[?] C. V[?] I D[?] LI[?] U[?] [?] CHO, TA C[?] N X[?] C[?] [?] NH  
B[?] NH XE D[?] A TR[?] N V[?] NT[?] C C[?] A XE HO[?] C V[?] NT[?] C G[?] C C[?] A B[?] NH XE.

L M TH N O X C NH GIA T C C A XE TRONG TR NG H P N

GIA T? C C? A XE C? TH? ? ? ? C X? C? ? NH D? A TR? NS? THAY ? ? I V? N T? C THEO TH? I GIAN HO? C D  
TH? C? ? NG L? ? NG V? MOMEN QUAY. N? U B I? T V? N T? C V? TH? I GIAN THAY ? ? I, TA C? TH? D? NG C?  
ΔT. TRONG B? I N? Y, C? N L I? N H? G I? A C? C V? N T? C V? MOMEN QUAY ? ? T? NH GIA T? C.

L M T H N O P X C P NH MOMEN QU N T NH C A B NH XE TRONG B  
N Y

MOMEN QU<sup>2</sup> N T<sup>2</sup> NH C<sup>2</sup> A B<sup>2</sup> NH XE V<sup>2</sup> I KH<sup>2</sup> I L<sup>2</sup> <sup>2</sup> NG V<sup>2</sup> B<sup>2</sup> N K<sup>2</sup> NH CHO B<sup>2</sup> I C<sup>2</sup> NG TH<sup>2</sup> C I = (1/2) m R<sup>2</sup> N<sup>2</sup> U B<sup>2</sup> H<sup>2</sup> NH TR<sup>2</sup> <sup>2</sup> <sup>2</sup> C, HO<sup>2</sup> C C<sup>2</sup> NG TH<sup>2</sup> C PH<sup>2</sup> H<sup>2</sup> P T<sup>2</sup> Y D<sup>2</sup> NG B<sup>2</sup> NH XE. V<sup>2</sup> I M = 5KG V<sup>2</sup> R = 8CM, TA T<sup>2</sup> NH I = (1/ (0,08)<sup>2</sup> KG.M<sup>2</sup>.

L M T H N O P Q X C P NH L C T C D NG L N XE KHI B NH XE QUAY  
D L U CHO?

L[ ] C T[ ] C D[ ] NG C[ ] TH[ ] [ ] [ ] [ ] C X[ ] C [ ] [ ] NH QUA [ ] [ ] NH LU[ ] T || NEWTON HO[ ] C QUA MOMEN QUAY, D[ ] A TR[ ]  
MOMEN QU[ ] N T[ ] NH. N[ ] U BI[ ] T T[ ] C [ ] [ ] V[ ] GIA T[ ] C, TA C[ ] TH[ ] T[ ] NH L[ ] C B[ ] NG F = M A, [ ] [ ] NG TH[ ] I XEM  
QUAY T[ ] C D[ ] NG L[ ] N B[ ] NH XE [ ] [ ] GI[ ] I B[ ] I TO[ ] N CH[ ] NH X[ ] C.

☐ NGH ☐ A C ☐ A G ☐ C N ☐ M TR ☐ N M ☐ T TRONG B ☐ I TO ☐ N N ☐ Y L ☐ G ☐ ?

G? C N? M TR? N M? T TH? HI? N H? ? NG C? A L? C HO? C V? N T? C LI? N QUAN? ? N M? T PH? NG NGANG HO?  
 ? ? N C? CH T? NH C? C TH? NH PH? N L? C T? C D? NG, GIA T? C V? CHUY? N ? ? NG C? A XE. VI? C X? C ? ?  
 ? ? NH PH? N T? CH L? C CH? NH X? CH? N.

C B C N TH C HI N GI I QUY T B I TO N V CHUY N  
B NH XE TRONG B I N Y L G ?

C B C BAO G M: X C NH C C D KI N V KH I L NG, B N K NH, V N T C; T NH TO N MO  
B NH XE; X C NH V N T C, GIA T C C A XE D A TR N C C D KI N; PH N T CH L C V MOMEN T  
C NG, P D NG C C NG TH C NG L C T M R A C I L NG C N TH T TRONG B I TO

## ADDITIONAL RESOURCES

MT BNH XE BAO GM 1 VNH BNH XE C KHI LNG M=5KG V 8 CM, MI CM C KHI LNG M=1KG V DI R=0,4M, ANG LN TRN MT

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## INTRODUCTION

IN THE REALM OF PHYSICS AND ENGINEERING, UNDERSTANDING THE BEHAVIOR OF OBJECTS IN MOTION IS ESSENTIAL FOR DESIGNING SYSTEMS RANGING FROM SIMPLE MECHANICAL DEVICES TO COMPLEX AEROSPACE STRUCTURES. TODAY, WE DELVE INTO A

DETAILED ANALYSIS OF A SPECIFIC MECHANICAL SETUP INVOLVING TWO CONTAINERS OF DIFFERENT MASSES, VOLUMES, AND MOTION CHARACTERISTICS — AN INTRIGUING SCENARIO THAT EXEMPLIFIES CORE PRINCIPLES SUCH AS CONSERVATION OF MOMENTUM, ENERGY TRANSFER, AND ROTATIONAL DYNAMICS.

THIS ARTICLE AIMS TO PROVIDE AN IN-DEPTH EXPLORATION OF THE PROBLEM STATEMENT, BREAKING DOWN EACH COMPONENT, THEIR INTERACTIONS, AND THE UNDERLYING PHYSICS PRINCIPLES. WHETHER YOU'RE A STUDENT, EDUCATOR, OR ENGINEERING ENTHUSIAST, THIS COMPREHENSIVE REVIEW WILL ENHANCE YOUR UNDERSTANDING OF DYNAMIC SYSTEMS INVOLVING MASS, VOLUME, AND ANGULAR MOTION.

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## CLARIFYING THE PROBLEM: DECODING THE PARAMETERS

BEFORE PROCEEDING, IT'S CRUCIAL TO INTERPRET AND CLARIFY THE PARAMETERS PROVIDED, AS THE INITIAL DESCRIPTION SEEMS TO INCLUDE SOME ABBREVIATIONS AND POSSIBLY TYPOGRAPHICAL INCONSISTENCIES. BASED ON CONTEXT AND COMMON PHYSICS NOTATION, HERE'S A LIKELY INTERPRETATION:

- "Mt Bnh Xe Bao Gm 1 Vnh Bnh Xe": POSSIBLY REFERS TO A CONTAINER OR VESSEL ("Bể" NH XE" IN VIETNAMESE), WITH CERTAIN MASS AND VOLUME CHARACTERISTICS.
- "C Khi Lng M=5kg V 8 Cm": A BODY OR FLUID WITH MASS  $(M = 5\text{ kg})$ , VOLUME  $(V = 8\text{ cm}^3)$ .
- "Mi Cm C Khi Lng M=1kg V Di R=0,4m": ANOTHER MASS  $(m = 1\text{ kg})$ , WITH SOME CHARACTERISTIC LENGTH OR DISPLACEMENT  $(R = 0.4\text{ m})$ . THE "Mi Cm" MAY DENOTE THE INITIAL POSITION OR A PARAMETER RELATED TO THE SYSTEM.
- "Ang Ln Trn Mt": POSSIBLY REFERRING TO AN ANGLE  $(\theta)$  (ANGULAR POSITION) RELATIVE TO A REFERENCE POINT OR AXIS.

GIVEN THESE INTERPRETATIONS, THE CORE COMPONENTS OF THE SYSTEM INVOLVE:

1. A CONTAINER OR VESSEL WITH SPECIFIC MASS AND VOLUME.
2. A FLUID OR OBJECT OF MASS 5 KG AND VOLUME 8 CM<sup>3</sup>.
3. A SMALLER MASS OF 1 KG, LOCATED AT A DISTANCE  $(R = 0.4\text{ m})$  FROM A PIVOT OR AXIS.
4. ANGULAR CONSIDERATIONS, PERHAPS INVOLVING THE TILT OR ROTATION OF THE SYSTEM.

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## PHYSICAL COMPONENTS AND ASSUMPTIONS

TO ANALYZE THIS SCENARIO THOROUGHLY, LET'S ASSUME THE FOLLOWING:

- THE SYSTEM INVOLVES A ROTATING OR PIVOTED CONTAINER (POSSIBLY A LEVER OR ARM) WITH A MASS  $(M)$  LOCATED AT A DISTANCE  $(R)$ .
- THE FLUID OR MATERIAL WITH MASS  $(M)$  AND VOLUME  $(V)$  CONTRIBUTES TO THE SYSTEM'S MASS DISTRIBUTION.
- THE ANGLE  $(\theta)$  REPRESENTS THE TILT OR INCLINATION OF THE SYSTEM, AFFECTING THE TORQUE AND EQUILIBRIUM.

KEY ASSUMPTIONS FOR SIMPLIFICATION:

- THE SYSTEM IS ISOLATED, WITH NO EXTERNAL FORCES BESIDES GRAVITY.
- THE MASS OF THE CONTAINER ITSELF IS NEGLIGIBLE OR INCLUDED IN THE GIVEN PARAMETERS.
- THE FLUID IS INCOMPRESSIBLE, AND ITS VOLUME REMAINS CONSTANT.
- THE MOTION CONSIDERED IS PRIMARILY ROTATIONAL, WITH POSSIBLE OSCILLATIONS OR STATIC EQUILIBRIUM.

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## ANALYZING THE SYSTEM: FUNDAMENTAL PHYSICS PRINCIPLES

### 1. CONSERVATION OF MOMENTUM AND ENERGY

THE INTERPLAY BETWEEN THE MASSES INVOLVES BOTH LINEAR AND ANGULAR MOMENTUM. WHEN THE SMALLER MASS  $(m)$  MOVES OR THE CONTAINER TILTS, THE SYSTEM'S ENERGY SHIFTS BETWEEN POTENTIAL AND KINETIC FORMS.

## 2. TORQUE AND ROTATIONAL EQUILIBRIUM

THE ANGULAR POSITION  $\theta$  IS GOVERNED BY THE TORQUES ACTING ON THE SYSTEM:

$$\tau = r \times F$$

WHERE:

- $r$  IS THE DISTANCE FROM THE PIVOT POINT (HERE,  $r = 0.4 \text{ m}$ )
- $F$  IS THE FORCE DUE TO GRAVITY ACTING ON THE MASS OR FLUID.

THE NET TORQUE DETERMINES WHETHER THE SYSTEM REMAINS IN EQUILIBRIUM OR OSCILLATES.

## 3. CENTER OF MASS CONSIDERATIONS

THE OVERALL STABILITY DEPENDS ON THE POSITION OF THE COMBINED CENTER OF MASS, WHICH IS AFFECTED BY:

- THE MASS DISTRIBUTION OF THE CONTAINER AND FLUID.
- THE POSITION OF THE SMALLER MASS  $m$ .

CALCULATING THE CENTER OF MASS ENABLES PREDICTION OF THE SYSTEM'S TENDENCY TO TILT OR RETURN TO EQUILIBRIUM.

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### DETAILED CALCULATIONS AND MODELING

#### A. MASS AND VOLUME RELATIONSHIP

GIVEN:

- $M = 5 \text{ kg}$
- $V = 8 \text{ cm}^3 = 8 \times 10^{-6} \text{ m}^3$

THE DENSITY OF THE FLUID OR OBJECT:

$$\rho = \frac{M}{V} = \frac{5 \text{ kg}}{8 \times 10^{-6} \text{ m}^3} = 6.25 \times 10^5 \text{ kg/m}^3$$

THIS HIGH DENSITY SUGGESTS A DENSE MATERIAL, POSSIBLY METAL OR A DENSE FLUID.

#### B. MOMENT OF INERTIA

THE ROTATIONAL DYNAMICS DEPEND ON THE MOMENT OF INERTIA  $I$ . FOR A POINT MASS  $m$  AT RADIUS  $r$ :

$$I = m r^2 = 1 \text{ kg} \times (0.4 \text{ m})^2 = 0.16 \text{ kg} \cdot \text{m}^2$$

IF CONSIDERING THE ENTIRE SYSTEM, THE CONTAINER'S INERTIA AND FLUID'S CONTRIBUTION MUST BE INCLUDED, WHICH CAN BE COMPLEX DEPENDING ON SHAPE.

#### C. TORQUE CALCULATION

THE TORQUE EXERTED BY THE MASS  $m$ :

$$\tau$$

$$\tau = m g R \sin \theta$$

Where  $(g \approx 9.81 \text{ m/s}^2)$ .

The torque due to the fluid or container's weight depends on the center of mass position and can be similarly calculated.

#### D. EQUILIBRIUM CONDITIONS

At equilibrium, the net torque is zero:

$$\sum \tau = 0$$

This condition allows solving for the equilibrium angle  $(\theta)$ .

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#### EXPLORING THE ANGULAR MOTION: $\theta$ vs $t$

The phrase " $\theta$  vs  $t$ " likely refers to the angle of tilt or the angle of inclination of the system.

##### 1. SMALL ANGLE APPROXIMATION

For small  $(\theta)$ :

$$\sin \theta \approx \theta$$

This simplifies calculations and is typical in analyzing oscillations or stability.

##### 2. OSCILLATORY BEHAVIOR

If displaced from equilibrium, the system may exhibit oscillations characterized by:

$$\omega = \sqrt{\frac{k}{I}}$$

Where  $(k)$  is the effective torsional stiffness, derived from the restoring torque per unit angular displacement.

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#### PRACTICAL IMPLICATIONS AND APPLICATIONS

Understanding such systems is vital in various engineering fields:

- DESIGNING BALANCED ROTATING MACHINERY: Ensuring stability by analyzing mass distribution and moments.
- FLUID MECHANICS IN ROTATING CONTAINERS: Predicting fluid behavior (e.g., in centrifuges).
- ROBOTICS: Balancing arms with discrete masses.
- AEROSPACE ENGINEERING: Attitude control involving mass and inertia management.

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#### SUMMARY OF KEY INSIGHTS

- THE SYSTEM'S BEHAVIOR HINGES ON THE DISTRIBUTION OF MASS, THE GEOMETRY (DISTANCES LIKE  $(R)$ ), AND THE ANGULAR POSITION  $(\theta)$ .
- CALCULATIONS OF TORQUE, MOMENT OF INERTIA, AND CENTER OF MASS ARE ESSENTIAL FOR UNDERSTANDING STABILITY.
- SMALL ANGULAR DISPLACEMENTS CAN BE APPROXIMATED LINEARLY, ENABLING EASIER ANALYSIS OF OSCILLATIONS.
- THE HIGH DENSITY OF THE FLUID SUGGESTS CAREFUL CONSIDERATION OF INTERNAL FORCES AND POTENTIAL FLUID-STRUCTURE INTERACTIONS.

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## FINAL THOUGHTS

ANALYZING A COMPLEX SYSTEM INVOLVING MULTIPLE MASSES, VOLUMES, AND ROTATIONAL DYNAMICS REQUIRES A MULTIFACETED APPROACH GROUNDED IN CORE PHYSICS PRINCIPLES. BY DISSECTING EACH COMPONENT, CALCULATING MOMENTS, TORQUES, AND EQUILIBRIUM CONDITIONS, ENGINEERS AND PHYSICISTS CAN OPTIMIZE SYSTEMS FOR STABILITY AND PERFORMANCE.

THIS DETAILED REVIEW UNDERSCORES THE IMPORTANCE OF PRECISE PARAMETER INTERPRETATION AND SYSTEMATIC ANALYSIS IN UNDERSTANDING REAL-WORLD MECHANICAL SYSTEMS. WHETHER FOR ACADEMIC RESEARCH, PRODUCT DEVELOPMENT, OR EDUCATIONAL PURPOSES, MASTERING THESE CONCEPTS EQUIPS PRACTITIONERS TO TACKLE A WIDE ARRAY OF ENGINEERING CHALLENGES.

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NOTE: FOR A COMPREHENSIVE UNDERSTANDING, FURTHER EXPERIMENTAL DATA OR DETAILED SCHEMATICS WOULD ENHANCE THE ANALYSIS. IF SPECIFIC SYSTEM CONFIGURATIONS, CONSTRAINTS, OR ADDITIONAL PARAMETERS ARE AVAILABLE, THEY SHOULD BE INCORPORATED FOR MORE PRECISE MODELING.

## **Mt Bnh Xe Bao Gm 1 Vnh Bnh Xe C Khi Lng M 5kg V 8 Cm Mi Cm C Khi Lng M 1kg V Di R 0 4m Ang Ln Trn Mt**

Mt Bnh Xe Bao Gm 1 Vnh Bnh Xe C Khi Lng M 5kg V 8 Cm Mi Cm C Khi Lng M 1kg V Di R 0 4m Ang Ln Trn Mt

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