

A 208-V, Two-pole, 60-Hz Y-Connected Wound-Rotor Induction Motor Is Rated At 15 Hp. Its Equivalent Circuit

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Understanding the operation and design of induction motors is essential for electrical engineers, technicians, and students involved in motor applications. Among various types of induction motors, the wound-rotor induction motor stands out due to its controllability and adaptability in industrial settings. In this article, we explore the detailed aspects of a typical 208-volt, two-pole, 60-Hz Y-connected wound-rotor induction motor rated at 15 horsepower, focusing particularly on its equivalent circuit. This analysis provides insight into how the motor functions, how its parameters are modeled, and how these models are used for performance prediction and troubleshooting.

Overview of Wound-Rotor Induction Motors

What Is a Wound-Rotor Induction Motor?

A wound-rotor induction motor is a type of squirrel-cage motor where the rotor windings are made of insulated wire coils, similar to the stator windings. These rotor windings are connected to external resistors or controllers via slip rings and brushes, allowing for variable resistance in the rotor circuit. This configuration enhances starting torque, reduces starting current, and provides a means for speed control.

Advantages of Wound-Rotor Motors

- High starting torque
- Adjustable speed operation
- Reduced starting current
- Flexibility in controlling motor performance

Applications

- Heavy-duty hoists and cranes
- Conveyors
- Crushers
- Pumps requiring adjustable speed and high torque

Specifications of the Motor

Before delving into the equivalent circuit, it's important to understand the key parameters and specifications of the motor under consideration:

- Voltage: 208 V (Line-to-Line)

- NUMBER OF POLES: 2
- FREQUENCY: 60 Hz
- CONNECTION: WYE (Y)
- POWER RATING: 15 Hp
- TYPE: WOUND-ROTOR INDUCTION MOTOR

GIVEN THESE SPECIFICATIONS, THE MOTOR OPERATES AT A SYNCHRONOUS SPEED THAT CAN BE CALCULATED, AND ITS EQUIVALENT CIRCUIT PARAMETERS CAN BE MODELED ACCORDINGLY.

CALCULATING SYNCHRONOUS SPEED

THE SYNCHRONOUS SPEED (N_s) FOR A MOTOR IS GIVEN BY:

$$N_s = (120 \times \text{FREQUENCY}) / \text{NUMBER OF POLES}$$

PLUGGING IN THE VALUES:

$$N_s = (120 \times 60 \text{ Hz}) / 2 = 3600 / 2 = 1800 \text{ RPM}$$

THIS IS THE THEORETICAL MAXIMUM SPEED OF THE MOTOR IN THE ABSENCE OF SLIP.

UNDERSTANDING THE EQUIVALENT CIRCUIT

WHAT IS AN EQUIVALENT CIRCUIT?

AN EQUIVALENT CIRCUIT IS A SIMPLIFIED ELECTRICAL MODEL THAT REPRESENTS THE COMPLEX INDUCTIVE AND RESISTIVE BEHAVIORS OF THE MOTOR'S STATOR AND ROTOR. IT ALLOWS ENGINEERS TO ANALYZE PERFORMANCE CHARACTERISTICS SUCH AS TORQUE, POWER FACTOR, EFFICIENCY, AND STARTING BEHAVIOR.

COMPONENTS OF THE WOUND-ROTOR EQUIVALENT CIRCUIT

THE TYPICAL EQUIVALENT CIRCUIT OF A WOUND-ROTOR INDUCTION MOTOR INCLUDES:

- STATOR RESISTANCE (R_s) AND REACTANCE (X_s): REPRESENTING THE STATOR WINDING LOSSES AND LEAKAGE REACTANCE.
- ROTOR RESISTANCE (R_r) AND REACTANCE (X_r): REPRESENTING THE ROTOR'S EQUIVALENT RESISTANCE AND LEAKAGE REACTANCE REFERRED TO THE STATOR SIDE.
- MAGNETIZING BRANCH: REPRESENTING THE MAGNETIZING CURRENT AND CORE LOSSES.
- EXTERNAL RESISTANCE (R_g): CONNECTED IN SERIES WITH THE ROTOR CIRCUIT VIA SLIP RINGS FOR CONTROL.

THESE COMPONENTS ARE INTERCONNECTED TO SIMULATE THE MOTOR'S BEHAVIOR AT VARIOUS SLIP VALUES.

DERIVING THE EQUIVALENT CIRCUIT PARAMETERS

STATOR PARAMETERS

- STATOR RESISTANCE (R_s): ACCOUNTS FOR THE COPPER LOSSES IN THE STATOR WINDINGS.
- STATOR REACTANCE (X_s): ACCOUNTS FOR LEAKAGE FLUX ASSOCIATED WITH THE STATOR WINDING.

ROTOR PARAMETERS

- ROTOR RESISTANCE (R_r): REFLECTS THE ROTOR COPPER LOSSES.
- ROTOR REACTANCE (X_r): ACCOUNTS FOR LEAKAGE FLUX IN THE ROTOR CIRCUIT.

MAGNETIZING BRANCH

- MAGNETIZING REACTANCE (X_m): MODELS THE MAGNETIZING CURRENT NECESSARY TO ESTABLISH THE MAGNETIC FLUX.
- CORE LOSS RESISTANCE (R_c): REPRESENTS CORE LOSSES SUCH AS HYSTERESIS AND EDDY CURRENTS.

EXTERNAL RESISTANCE (R_g)

THIS IS THE RESISTANCE ADDED IN SERIES TO CONTROL STARTING TORQUE AND CURRENT. IT CAN BE VARIED DURING MOTOR STARTUP AND OPERATION.

CONSTRUCTING THE EQUIVALENT CIRCUIT

THE EQUIVALENT CIRCUIT CAN BE REPRESENTED AS FOLLOWS:

- THE STATOR IMPEDANCE ($R_s + jX_s$) IN SERIES WITH
- THE PARALLEL MAGNETIZING BRANCH (R_c AND X_m)
- THE ROTOR BRANCH ($R_r / s + jX_r$) REFERRED TO THE STATOR SIDE
- EXTERNAL ROTOR RESISTANCE R_g IN SERIES WITH THE ROTOR BRANCH

THE CIRCUIT DIAGRAM FACILITATES THE CALCULATION OF VARIOUS OPERATIONAL PARAMETERS AT DIFFERENT SLIPS.

MATHEMATICAL REPRESENTATION OF THE EQUIVALENT CIRCUIT

THE KEY EQUATIONS INVOLVE CALCULATING THE MOTOR'S TORQUE, POWER FACTOR, AND EFFICIENCY. THE MAIN VARIABLES INCLUDE:

- SLIP (s): $s = (N_s - N_r) / N_s$
- ROTOR CIRCUIT IMPEDANCE (Z_r): $R_r / s + jX_r$
- ROTOR CURRENT (I_r): V_2 / Z_r
- ELECTROMAGNETIC TORQUE (T_e): PROPORTIONAL TO THE ROTOR CURRENT SQUARED AND THE ROTOR FLUX

THE APPROXIMATE EXPRESSION FOR THE TORQUE IS:

$$T \propto (s \times R_r \times |I_r|^2)$$

THIS RELATIONSHIP INDICATES THAT TORQUE VARIES WITH SLIP AND RESISTANCES IN THE ROTOR CIRCUIT.

PERFORMANCE ANALYSIS USING THE EQUIVALENT CIRCUIT

STARTING CONDITIONS (SLIP $s = 1$)

- ROTOR RESISTANCE DOMINATES THE IMPEDANCE
- HIGH STARTING TORQUE ACHIEVABLE WITH MINIMAL ROTOR RESISTANCE
- LARGE ROTOR CURRENT, LEADING TO HIGH STARTING TORQUE

RUNNING CONDITIONS (SLIP $s < 1$)

- ROTOR IMPEDANCE DECREASES AS SLIP DECREASES
- POWER TRANSFER FROM STATOR TO ROTOR ADJUSTS ACCORDINGLY
- EFFICIENCY IS MAXIMIZED AT A CERTAIN SLIP

IMPACT OF EXTERNAL ROTOR RESISTANCE

ADDING EXTERNAL RESISTANCE R_g AFFECTS STARTING TORQUE AND SPEED CONTROL:

- INCREASED R_g IMPROVES STARTING TORQUE
- EXCESSIVE RESISTANCE REDUCES MAXIMUM TORQUE AND EFFICIENCY
- PROPER SIZING OF R_g IS ESSENTIAL FOR OPTIMAL PERFORMANCE

APPLICATION OF THE EQUIVALENT CIRCUIT IN MOTOR ANALYSIS

THE EQUIVALENT CIRCUIT SERVES AS AN ESSENTIAL TOOL FOR:

- PREDICTING STARTING TORQUE AND CURRENT
- ANALYZING SPEED-TORQUE CHARACTERISTICS
- CALCULATING POWER LOSSES AND EFFICIENCY
- DESIGNING CONTROL SCHEMES FOR VARIABLE SPEED APPLICATIONS

CONCLUSION

THE 208-V, TWO-POLE, 60-Hz WOUND-ROTOR INDUCTION MOTOR RATED AT 15 HP EXEMPLIFIES THE PRACTICAL USE OF EQUIVALENT CIRCUIT MODELING. BY UNDERSTANDING AND ANALYZING ITS EQUIVALENT CIRCUIT, ENGINEERS CAN OPTIMIZE PERFORMANCE, ENHANCE CONTROL STRATEGIES, AND TROUBLESHOOT OPERATIONAL ISSUES EFFECTIVELY. THE EQUIVALENT CIRCUIT PROVIDES A BRIDGE BETWEEN THE COMPLEX ELECTROMAGNETIC PHENOMENA IN THE MOTOR AND THE SIMPLIFIED ELECTRICAL MODELS NECESSARY FOR PRACTICAL ANALYSIS. WHETHER DESIGNING NEW SYSTEMS OR MAINTAINING EXISTING ONES, MASTERING THE EQUIVALENT CIRCUIT OF WOUND-ROTOR INDUCTION MOTORS IS VITAL FOR EFFICIENT AND RELIABLE MOTOR OPERATION.

KEYWORDS: WOUND-ROTOR INDUCTION MOTOR, EQUIVALENT CIRCUIT, 15 HP MOTOR, 208 V MOTOR, TWO-POLE MOTOR, 60 HZ MOTOR, SLIP, MOTOR PERFORMANCE, EQUIVALENT CIRCUIT PARAMETERS, MOTOR ANALYSIS, SPEED CONTROL

FREQUENTLY ASKED QUESTIONS

WHAT IS THE SIGNIFICANCE OF THE 208-V RATING IN A TWO-POLE, 60-Hz Y-CONNECTED WOUND-ROTOR INDUCTION MOTOR?

THE 208-V RATING INDICATES THE LINE-TO-LINE VOLTAGE SUPPLIED TO THE MOTOR, WHICH INFLUENCES THE MOTOR'S VOLTAGE, CURRENT, AND POWER RATINGS, ENSURING PROPER OPERATION AND PERFORMANCE WITHIN SPECIFIED LIMITS.

HOW DOES THE TWO-POLE DESIGN AFFECT THE PERFORMANCE OF THE 15 HP WOUND-ROTOR INDUCTION MOTOR?

A TWO-POLE DESIGN RESULTS IN A HIGH SYNCHRONOUS SPEED (AROUND 3600 RPM AT 60 Hz), ENABLING THE MOTOR TO ACHIEVE HIGH ROTATIONAL SPEEDS SUITABLE FOR APPLICATIONS REQUIRING RAPID ACCELERATION AND HIGH-SPEED OPERATION.

WHAT IS MEANT BY THE MOTOR BEING Y-CONNECTED, AND HOW DOES THIS IMPACT ITS EQUIVALENT CIRCUIT?

Y-CONNECTED (WYE-CONNECTED) MEANS THE MOTOR'S STATOR WINDINGS ARE CONNECTED IN A STAR CONFIGURATION, WHICH AFFECTS THE PHASE VOLTAGE, LINE-TO-LINE VOLTAGE, AND THE CALCULATION OF THE MOTOR'S EQUIVALENT CIRCUIT PARAMETERS, INCLUDING IMPEDANCE AND MAGNETIZING REACTANCE.

HOW IS THE RATED POWER OF 15 HP REFLECTED IN THE EQUIVALENT CIRCUIT PARAMETERS?

THE RATED POWER INFLUENCES THE MOTOR'S IMPEDANCE VALUES, CORE LOSSES, AND MAGNETIZING REACTANCE IN THE EQUIVALENT CIRCUIT, WHICH COLLECTIVELY DETERMINE THE MOTOR'S OPERATIONAL CHARACTERISTICS AT RATED LOAD.

WHAT COMPONENTS ARE TYPICALLY INCLUDED IN THE EQUIVALENT CIRCUIT OF A WOUND-ROTOR INDUCTION MOTOR?

THE EQUIVALENT CIRCUIT GENERALLY INCLUDES STATOR RESISTANCE AND REACTANCE, MAGNETIZING REACTANCE, ROTOR RESISTANCE AND REACTANCE REFERRED TO THE STATOR SIDE, AND THE CORE LOSS RESISTANCE, REPRESENTING ALL MAIN ENERGY TRANSFER AND LOSS MECHANISMS.

WHY IS THE EQUIVALENT CIRCUIT IMPORTANT FOR ANALYZING THE PERFORMANCE OF A 15 HP WOUND-ROTOR INDUCTION MOTOR?

THE EQUIVALENT CIRCUIT ALLOWS ENGINEERS TO CALCULATE KEY PERFORMANCE PARAMETERS SUCH AS STARTING TORQUE, MAXIMUM TORQUE, SLIP, EFFICIENCY, AND POWER FACTOR, FACILITATING EFFECTIVE DESIGN, CONTROL, AND TROUBLESHOOTING.

HOW DOES THE OPERATING FREQUENCY OF 60 Hz AFFECT THE IMPEDANCE COMPONENTS IN THE EQUIVALENT CIRCUIT?

THE FREQUENCY INFLUENCES THE INDUCTIVE REACTANCES IN THE CIRCUIT, AS REACTANCE (X) IS PROPORTIONAL TO FREQUENCY ($X = 2\pi fL$), IMPACTING THE IMPEDANCE AND THUS THE MOTOR'S TORQUE AND CURRENT CHARACTERISTICS.

WHAT ROLE DOES THE WOUND-ROTOR DESIGN PLAY IN THE EQUIVALENT CIRCUIT ANALYSIS OF THIS MOTOR?

THE WOUND-ROTOR ALLOWS EXTERNAL RESISTANCE TO BE ADDED IN THE ROTOR CIRCUIT, AFFECTING THE ROTOR IMPEDANCE, SLIP, AND TORQUE CHARACTERISTICS, WHICH ARE REPRESENTED IN THE EQUIVALENT CIRCUIT TO ANALYZE STARTING PERFORMANCE AND SPEED CONTROL.

HOW CAN THE EQUIVALENT CIRCUIT BE USED TO DETERMINE THE STARTING TORQUE OF THE MOTOR?

BY ANALYZING THE EQUIVALENT CIRCUIT AT ZERO SLIP (START), WHERE ROTOR IMPEDANCE IS PURELY RESISTANCE, YOU CAN CALCULATE THE STARTING TORQUE USING THE MOTOR'S PARAMETERS, PROVIDING INSIGHTS INTO ITS INITIAL ACCELERATION CAPABILITIES.

WHAT ARE COMMON METHODS TO DERIVE THE PARAMETERS OF THE EQUIVALENT CIRCUIT FOR A 15 HP WOUND-ROTOR INDUCTION MOTOR?

PARAMETERS ARE OFTEN OBTAINED THROUGH NO-LOAD AND LOCKED-ROTOR TESTS, USING STANDARD TEST DATA AND RATED OPERATING CONDITIONS TO CALCULATE RESISTANCES, REACTANCES, AND MAGNETIZING COMPONENTS FOR ACCURATE MODELING.

ADDITIONAL RESOURCES

A 208-V, TWO-POLE, 60-Hz Y-CONNECTED WOUND-ROTOR INDUCTION MOTOR IS RATED AT 15 HP. ITS EQUIVALENT CIRCUIT

INTRODUCTION TO WOUND-ROTOR INDUCTION MOTORS

WOUND-ROTOR INDUCTION MOTORS ARE A SPECIALIZED CLASS OF INDUCTION MOTORS DISTINGUISHED BY THEIR EXTERNAL ROTOR WINDINGS CONNECTED VIA SLIP RINGS AND BRUSHES. THEY ARE WIDELY USED IN APPLICATIONS REQUIRING HIGH STARTING TORQUE, CONTROLLED ACCELERATION, OR ADJUSTABLE SPEED. UNDERSTANDING THEIR EQUIVALENT CIRCUIT IS FUNDAMENTAL FOR ANALYZING PERFORMANCE, DIAGNOSING FAULTS, AND OPTIMIZING OPERATION.

THE SPECIFIC MOTOR IN FOCUS IS A 208-V, TWO-POLE, 60-Hz Y-CONNECTED WOUND-ROTOR INDUCTION MOTOR RATED AT 15 HP. THIS CONFIGURATION OFFERS INSIGHTS INTO THE MOTOR'S OPERATIONAL CHARACTERISTICS, ELECTRICAL PARAMETERS, AND PERFORMANCE MODELING.

BASIC CONSTRUCTION AND OPERATING PRINCIPLES

PHYSICAL STRUCTURE

- STATOR: CONTAINS THREE-PHASE WINDINGS CONNECTED IN A Y-CONFIGURATION, SUPPLIED WITH 208 V, 60 Hz POWER.
- ROTOR: WOUND WITH CONDUCTORS AND CONNECTED TO EXTERNAL RESISTANCES VIA SLIP RINGS AND BRUSHES, FACILITATING CONTROL OVER TORQUE AND SPEED.
- AIR GAP: CRITICAL FOR MAGNETIC FLUX LINKAGE; INFLUENCES MAGNETIZING CURRENT AND CORE LOSSES.

OPERATING PRINCIPLE

- WHEN THREE-PHASE AC SUPPLY ENERGIZES THE STATOR, A ROTATING MAGNETIC FIELD IS PRODUCED.
- THIS MAGNETIC FIELD INDUCES CURRENTS IN THE ROTOR CONDUCTORS (VIA ELECTROMAGNETIC INDUCTION), WHICH IN TURN PRODUCE THEIR OWN MAGNETIC FIELDS.
- THE INTERACTION BETWEEN STATOR AND ROTOR MAGNETIC FIELDS PRODUCES TORQUE.
- THE ROTOR'S SLIP, DEFINED AS $s = \frac{N_s - N_r}{N_s}$, DETERMINES THE ROTOR FREQUENCY AND CONSEQUENTLY THE TORQUE AND POWER FLOW.

ELECTRICAL SPECIFICATION AND RATINGS

- VOLTAGE: 208 V LINE-TO-LINE IN A Y-CONNECTION
- FREQUENCY: 60 Hz
- POLES: TWO, WHICH IMPLIES A SYNCHRONOUS SPEED OF APPROXIMATELY 3600 RPM (ASSUMING NO LOAD AND NEGLIGIBLE SLIP)
- HORSEPOWER: 15 Hp (APPROX. 11.19 kW)
- RATED POWER: POWER DELIVERED AT RATED CONDITIONS, CONSIDERING EFFICIENCY AND POWER FACTOR

THE RATED VOLTAGE, FREQUENCY, AND POLE COUNT ARE ESSENTIAL FOR CALCULATING THE SYNCHRONOUS SPEED AND UNDERSTANDING THE MOTOR'S PERFORMANCE ENVELOPES.

UNDERSTANDING THE EQUIVALENT CIRCUIT CONCEPT

AN EQUIVALENT CIRCUIT SIMPLIFIES THE COMPLEX ELECTROMAGNETIC PHENOMENA WITHIN THE MOTOR INTO AN ELECTRICAL CIRCUIT MODEL. THIS MODEL CAPTURES THE ESSENTIAL PARAMETERS INFLUENCING TORQUE, CURRENT, POWER FACTOR, EFFICIENCY, AND STARTING CHARACTERISTICS.

OBJECTIVES OF THE EQUIVALENT CIRCUIT:

- FACILITATE ANALYSIS OF MOTOR PERFORMANCE
- PREDICT RESPONSES UNDER VARYING LOAD CONDITIONS
- ASSIST IN FAULT DIAGNOSIS AND OPTIMIZATION

COMPONENTS OF THE WOUND-ROTOR INDUCTION MOTOR EQUIVALENT CIRCUIT

THE EQUIVALENT CIRCUIT TYPICALLY COMPRISES SEVERAL KEY ELEMENTS:

1. MAGNETIZING BRANCH

- MAGNETIZING REACTANCE (X_m): REPRESENTS THE MAGNETIZING CURRENT NEEDED TO ESTABLISH THE MAGNETIC FLUX.
- CORE LOSS RESISTANCE (R_c): ACCOUNTS FOR CORE HYSTERESIS AND EDDY CURRENT LOSSES.

2. STATOR IMPEDANCE

- STATOR RESISTANCE (R_s): RESISTANCE OF THE STATOR WINDING CONDUCTORS.
- STATOR LEAKAGE REACTANCE (X_s): REPRESENTS LEAKAGE FLUX AROUND THE STATOR WINDING.

3. ROTOR CIRCUIT (REFLECTED TO STATOR SIDE)

- ROTOR RESISTANCE (R_r'): RESISTANCE OF THE ROTOR CONDUCTORS, REFLECTED TO THE STATOR SIDE.
- ROTOR LEAKAGE REACTANCE (X_r'): ROTOR LEAKAGE REACTANCE, ALSO REFLECTED TO THE STATOR SIDE.
- ROTOR RESISTANCE WITH EXTERNAL RESISTANCE ($R_r' + R_{ext}$): ADJUSTABLE FOR STARTING TORQUE CONTROL.

CONSTRUCTING THE EQUIVALENT CIRCUIT FOR THE 15 HP WOUND-ROTOR MOTOR

STEP 1: DETERMINE RATED PARAMETERS

- LINE-TO-LINE VOLTAGE (V_L): 208 V
- LINE-TO-LINE VOLTAGE IN Y-CONNECTION: CONVERT TO PHASE VOLTAGE:

$$V_{PH} = \frac{V_L}{\sqrt{3}} \approx \frac{208}{1.732} \approx 120 \text{ V}$$

- RATED POWER: 15 HP $\approx 11.19 \text{ kW}$

STEP 2: CALCULATE SYNCHRONOUS SPEED

- FOR A TWO-POLE MOTOR:

$$N_s = \frac{120 \times f}{P} = \frac{120 \times 60}{2} = 3600 \text{ RPM}$$

STEP 3: OBTAIN OR ESTIMATE PARAMETERS

- THE ACTUAL PARAMETERS SUCH AS R_s , X_s , R_r' , X_r' , R_c , AND X_m ARE TYPICALLY OBTAINED FROM MANUFACTURER DATASHEETS, TEST DATA, OR STANDARD ESTIMATIONS BASED ON MOTOR SIZE.

STEP 4: MODEL SIMPLIFICATIONS

- ASSUME A STEADY-STATE SINUSOIDAL OPERATION.
- USE TYPICAL RATIOS FOR SIMILAR MOTORS IF SPECIFIC DATA ISN'T AVAILABLE.
- FOR A 15 HP MOTOR, TYPICAL VALUES MIGHT BE:
- R_s : SMALL, AROUND 0.1Ω
- X_s : AROUND 0.3Ω
- R_r' : VARIABLE DEPENDING ON EXTERNAL RESISTANCE, INITIALLY AROUND 0.2Ω
- X_r' : APPROXIMATELY 0.3Ω
- R_c : HIGH, AROUND 50Ω

- (X_M) : LARGE, AROUND 30Ω

FORMULATING THE EQUIVALENT CIRCUIT

THE EQUIVALENT CIRCUIT FOR A WOUND-ROTOR INDUCTION MOTOR, VIEWED FROM THE STATOR, IS TYPICALLY DRAWN AS FOLLOWS:

- A SERIES BRANCH CONTAINING (R_s) AND (X_s) .
- A PARALLEL MAGNETIZING BRANCH WITH (R_c) AND (X_M) .
- A ROTOR BRANCH REFLECTED TO THE STATOR SIDE WITH $(R_r' + R_{EXT})$ AND (X_r') .

DIAGRAMMATIC REPRESENTATION:

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V_PH --- R_s --- X_s ---+--- R_r' + R_EXT --- X_r' --- GROUND
|
R_c + jX_M
|
GROUND
'''
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NOTE: THE ROTOR RESISTANCE (R_r') IS ADJUSTED FOR EXTERNAL RESISTANCES DURING STARTING OR CONTROL CONDITIONS.

ANALYZING PERFORMANCE USING THE EQUIVALENT CIRCUIT

1. STARTING TORQUE

- MAXIMAL AT A CERTAIN ROTOR RESISTANCE.
- CONTROLLED BY ADDING EXTERNAL RESISTANCE IN ROTOR CIRCUIT.
- THE MODEL PREDICTS INITIAL TORQUE BY CALCULATING THE CURRENT WHEN SLIP (s) IS NEAR 1.

2. RUNNING CONDITIONS

- AS THE MOTOR REACHES NEAR SYNCHRONOUS SPEED, SLIP DECREASES, AND ROTOR FREQUENCY DROPS.
- POWER TRANSFER AND TORQUE DEPEND ON THE ROTOR RESISTANCE AND REACTANCE AT OPERATING SLIP.

3. POWER AND TORQUE CALCULATIONS

- POWER TRANSFERRED ACROSS THE AIR GAP:

$$P_r = 3 I_2^2 R_r'$$

- ELECTROMAGNETIC TORQUE:

$$T = \frac{P_R}{\omega_s} = \frac{3 R_R' I_2^2}{\omega_s}$$

- WHERE (I_2) IS THE ROTOR CURRENT, AND (ω_s) IS THE SYNCHRONOUS ANGULAR VELOCITY IN RAD/SEC.

4. EFFICIENCY AND POWER FACTOR

- EFFICIENCY DEPENDS ON THE RATIO OF OUTPUT POWER TO INPUT POWER.
- POWER FACTOR IS INFLUENCED BY THE MAGNETIZING REACTANCE AND RESISTANCES.

IMPLICATIONS FOR DESIGN AND OPERATION

STARTING AND CONTROL

- EXTERNAL ROTOR RESISTANCE CAN BE ADJUSTED TO OPTIMIZE STARTING TORQUE AND CURRENT.
- WOUND-ROTOR MOTORS ALLOW FOR SMOOTH ACCELERATION AND CONTROLLED TORQUE CURVES.

EFFICIENCY CONSIDERATIONS

- PROPER PARAMETER SELECTION ENSURES MINIMAL LOSSES.
- OVERDESIGNING MAGNETIZING REACTANCE CAN CAUSE HIGHER MAGNETIZING CURRENTS, REDUCING EFFICIENCY.

THERMAL AND MECHANICAL ASPECTS

- RESISTANCE HEATING IN ROTOR AND STATOR CONDUCTORS MUST BE MANAGED.
- ADEQUATE COOLING AND MATERIAL CHOICES ARE ESSENTIAL FOR SUSTAINED OPERATION.

PRACTICAL APPLICATION AND TESTING

TESTING METHODS

- NO-LOAD TEST: DETERMINES (R_c) AND (X_m) .
- LOCKED-ROTOR TEST: ESTIMATES (R_s) , (X_s) , (R_R') , AND (X_R') .
- EFFICIENCY CALCULATIONS INVOLVE LOAD TESTS MEASURING INPUT POWER, TORQUE, AND LOSSES.

PERFORMANCE CURVES

- TORQUE VS. SLIP.
- POWER FACTOR VS. SLIP.
- EFFICIENCY VS. LOAD.

ADJUSTMENTS AND TUNING

- ADDING EXTERNAL RESISTANCES DURING STARTUP.
- USING VARIABLE RESISTANCE TO OPTIMIZE TORQUE AND CURRENT.

CONCLUSION

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