

A STRESS OF 92 MPa IS APPLIED IN THE [0 0 1] DIRECTION OF A UNIT CELL OF A BCC IRON SINGLE CRYSTAL. CALCULATE

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INTRODUCTION

UNDERSTANDING THE BEHAVIOR OF SINGLE CRYSTALS UNDER APPLIED STRESS IS FUNDAMENTAL IN MATERIALS SCIENCE, ESPECIALLY FOR METALS LIKE IRON, WHICH CAN EXIST IN DIFFERENT CRYSTAL STRUCTURES SUCH AS BODY-CENTERED CUBIC (BCC). WHEN A UNIAXIAL STRESS IS APPLIED TO A SINGLE CRYSTAL, IT INFLUENCES THE CRYSTAL'S INTERNAL STRUCTURE, POTENTIALLY LEADING TO ELASTIC DEFORMATION, PLASTIC DEFORMATION, OR PHASE TRANSFORMATION.

IN THIS ARTICLE, WE EXAMINE THE PROBLEM OF APPLYING A 92 MPa STRESS IN THE [0 1 0] DIRECTION OF A BCC IRON SINGLE CRYSTAL. WE AIM TO CALCULATE THE RESULTING INTERNAL STRESSES, STRAINS, AND RELATED MECHANICAL RESPONSES OF THE CRYSTAL. THIS COMPREHENSIVE GUIDE COVERS THE NECESSARY CONCEPTS, EQUATIONS, AND STEP-BY-STEP CALCULATIONS TO UNDERSTAND THE MATERIAL'S BEHAVIOR UNDER THESE CONDITIONS.

UNDERSTANDING THE CRYSTAL STRUCTURE: BODY-CENTERED CUBIC (BCC) IRON

WHAT IS BCC IRON?

- BODY-CENTERED CUBIC (BCC) IS ONE OF THE COMMON CRYSTAL STRUCTURES OF IRON AT CERTAIN TEMPERATURES (BELOW 912°C).
- LATTICE PARAMETERS: THE UNIT CELL IS CUBIC WITH ATOMS AT EACH CORNER AND A SINGLE ATOM IN THE CENTER.
- ATOMIC ARRANGEMENT: ATOMS ARE ARRANGED IN A HIGHLY SYMMETRICAL PATTERN, LEADING TO ANISOTROPIC MECHANICAL PROPERTIES.

MECHANICAL ANISOTROPY IN BCC IRON

- THE ELASTIC AND PLASTIC RESPONSES DEPEND ON THE CRYSTALLOGRAPHIC DIRECTION DUE TO THE ANISOTROPIC NATURE OF THE CRYSTAL.
- DIFFERENT ORIENTATIONS (E.G., [100], [110], [111]) EXHIBIT DIFFERENT ELASTIC MODULI AND SLIP SYSTEMS.

FUNDAMENTAL CONCEPTS FOR STRESS AND STRAIN ANALYSIS

STRESS AND STRAIN TENSORS

- STRESS TENSOR (σ): DESCRIBES INTERNAL FORCES WITHIN A MATERIAL, EXPRESSED IN TERMS OF NORMAL AND SHEAR COMPONENTS.
- STRAIN TENSOR (ϵ): REPRESENTS DEFORMATION, CAPTURING HOW THE MATERIAL STRETCHES, COMPRESSES, OR SHEARS.

HOOKE'S LAW FOR ANISOTROPIC MATERIALS

FOR LINEAR ELASTIC MATERIALS, THE RELATIONSHIP BETWEEN STRESS AND STRAIN IS GIVEN BY THE GENERALIZED HOOKE'S LAW:

$$\begin{bmatrix} \sigma \\ \vdots \end{bmatrix} = \begin{bmatrix} C \\ \vdots \end{bmatrix} : \begin{bmatrix} \epsilon \\ \vdots \end{bmatrix}$$

OR INVERSELY,

$$\begin{bmatrix} \mathbf{\epsilon} \end{bmatrix} = \mathbf{S} : \mathbf{\sigma}$$

WHERE:

- $\mathbf{C}$ IS THE STIFFNESS TENSOR.
- $\mathbf{S}$ IS THE COMPLIANCE TENSOR (INVERSE OF STIFFNESS).

ELASTIC CONSTANTS OF BCC IRON

KNOWN ELASTIC MODULI

FOR BCC IRON AT ROOM TEMPERATURE, TYPICAL ELASTIC CONSTANTS (IN GPa) ARE:

ELASTIC CONSTANT	VALUE (GPa)	DESCRIPTION
C_{11}	230	NORMAL STIFFNESS IN [100]
C_{12}	135	COUPLING BETWEEN AXES
C_{44}	115	SHEAR STIFFNESS IN PLANES

NOTE: THESE VALUES ARE APPROXIMATE; ACTUAL VALUES MAY VARY BASED ON TEMPERATURE AND PURITY.

COMPLIANCE TENSOR COMPONENTS

THE COMPLIANCE TENSOR COMPONENTS ARE DERIVED FROM ELASTIC CONSTANTS:

$$S_{ij} = \text{INVERSE OF } C_{ij}$$

FOR CUBIC CRYSTALS, THE COMPLIANCE TENSOR IN VOIGT NOTATION SIMPLIFIES TO THREE INDEPENDENT COMPONENTS:

- $S_{11} = \frac{1}{C_{11}}$
- $S_{12} = -\frac{C_{12}}{C_{11}(C_{11} + 2C_{12})}$
- $S_{44} = \frac{1}{C_{44}}$

ALTERNATIVELY, THE FULL COMPLIANCE MATRIX IN VOIGT NOTATION IS:

$$\mathbf{S} = \begin{bmatrix} S_{11} & S_{12} & S_{12} & 0 & 0 & 0 \\ S_{12} & S_{11} & S_{12} & 0 & 0 & 0 \\ S_{12} & S_{12} & S_{11} & 0 & 0 & 0 \\ 0 & 0 & 0 & S_{44} & 0 & 0 \\ 0 & 0 & 0 & 0 & S_{44} & 0 \\ 0 & 0 & 0 & 0 & 0 & S_{44} \end{bmatrix}$$

APPLYING THE EXTERNAL STRESS: THE [0 1 0] DIRECTION

UNIAXIAL STRESS CONDITION

- THE APPLIED STRESS TENSOR σ IN THE CRYSTAL REFERS TO A UNIAXIAL STRESS OF 92 MPa IN THE $[0\ 1\ 0]$ DIRECTION.
- IN TENSOR FORM, ASSUMING THE PRINCIPAL AXIS ALIGNS WITH THE CRYSTAL AXES:

$$\sigma = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 92 & 0 \\ 0 & 0 & 0 \end{bmatrix} \text{ MPa}$$

SIGNIFICANCE OF THE $[0\ 1\ 0]$ DIRECTION

- THE $[0\ 1\ 0]$ DIRECTION CORRESPONDS TO THE Y-AXIS IN THE CRYSTAL COORDINATE SYSTEM.
- THE STRESS IS NORMAL STRESS ALONG THE Y-AXIS; SHEAR COMPONENTS ARE ZERO.

CALCULATING THE RESULTING STRAIN COMPONENTS

STEP 1: CONVERT STRESS TO CONSISTENT UNITS

- STRESS IS GIVEN IN MPa; ELASTIC CONSTANTS ARE IN GPa.
- CONVERT MPa TO GPa:

$$92 \text{ MPa} = 0.092 \text{ GPa}$$

STEP 2: CALCULATE STRAIN COMPONENTS USING COMPLIANCE TENSOR

THE STRAINS ARE CALCULATED AS:

$$\epsilon_i = \sum_j S_{ij} \sigma_j$$

GIVEN THE APPLIED UNIAXIAL STRESS, ONLY $\sigma_2 = 92 \text{ MPa}$ IS NON-ZERO.

STEP 3: DETERMINE THE STRAIN IN THE $[0\ 1\ 0]$ DIRECTION

THE NORMAL STRAIN IN THE Y-DIRECTION:

$$\epsilon_{yy} = S_{12} \sigma_{xx} + S_{11} \sigma_{yy} + S_{12} \sigma_{zz}$$

SINCE ONLY σ_{yy} IS NON-ZERO, THE OTHER STRESSES ARE ZERO, SO:

$$\epsilon_{yy} = S_{11} \times 0.092 \text{ GPa}$$

SIMILARLY, THE STRAINS IN THE X AND Z DIRECTIONS:

$$\begin{aligned} \backslash[\\ \backslash\text{VAREPSILON}_{\{xx\}} &= S_{\{12\}} \backslash\text{TIMES } 0.092 \backslash, \backslash\text{TEXT}\{\text{GPA}\} \\ \backslash] \\ \backslash[\\ \backslash\text{VAREPSILON}_{\{zz\}} &= S_{\{12\}} \backslash\text{TIMES } 0.092 \backslash, \backslash\text{TEXT}\{\text{GPA}\} \\ \backslash] \end{aligned}$$

SHEAR STRAINS ARE ZERO BECAUSE SHEAR STRESSES ARE ZERO.

COMPUTING THE COMPLIANCE COMPONENTS

USING THE ELASTIC CONSTANTS:

$$\backslash[\\ S_{\{11\}} = \backslash\text{FRAC}\{1\}\{C_{\{11\}}\} = \backslash\text{FRAC}\{1\}\{230 \backslash, \backslash\text{TEXT}\{\text{GPA}\}\} \backslash\text{APPROX } 4.3478 \backslash\text{TIMES } 10^{\{-3\}} \backslash, \backslash\text{TEXT}\{\text{GPA}\}^{\{-1\}} \\ \backslash]$$

$$\backslash[\\ S_{\{12\}} = -\backslash\text{FRAC}\{C_{\{12\}}\}\{C_{\{11\}}(C_{\{11\}} + 2C_{\{12\}})\} \\ \backslash]$$

CALCULATE DENOMINATOR:

$$\backslash[\\ C_{\{11\}} + 2C_{\{12\}} = 230 + 2 \backslash\text{TIMES } 135 = 230 + 270 = 500 \backslash, \backslash\text{TEXT}\{\text{GPA}\} \\ \backslash]$$

CALCULATE NUMERATOR:

$$\backslash[\\ C_{\{12\}} = 135 \backslash, \backslash\text{TEXT}\{\text{GPA}\} \\ \backslash]$$

THUS,

$$\backslash[\\ S_{\{12\}} = -\backslash\text{FRAC}\{135\}\{230 \backslash\text{TIMES } 500\} = -\backslash\text{FRAC}\{135\}\{115,000\} \backslash\text{APPROX } -1.1739 \backslash\text{TIMES } 10^{\{-3\}} \backslash, \\ \backslash\text{TEXT}\{\text{GPA}\}^{\{-1\}} \\ \backslash]$$

SIMILARLY,

$$\backslash[\\ S_{\{44\}} = \backslash\text{FRAC}\{1\}\{C_{\{44\}}\} = \backslash\text{FRAC}\{1\}\{115\} \backslash\text{APPROX } 8.6957 \backslash\text{TIMES } 10^{\{-3\}} \backslash, \backslash\text{TEXT}\{\text{GPA}\}^{\{-1\}} \\ \backslash]$$

FINAL STRAIN CALCULATIONS

NORMAL STRAINS:

$$\backslash[\\ \backslash\text{VAREPSILON}_{\{yy\}} = S_{\{11\}} \backslash\text{TIMES } 0.092 \backslash\text{APPROX } 4.3478 \backslash\text{TIMES } 10^{\{-3\}} \backslash\text{TIMES } 0.092 \backslash\text{APPROX } 4.0 \backslash\text{TIMES } 10^{\{-4\}} \\ \backslash]$$

$$\begin{aligned} \epsilon_{xx} = \epsilon_{zz} = S_{12} \times 0.092 \approx -1.1739 \times 10^{-3} \times 0.092 \\ \approx -1.08 \times 10^{-4} \end{aligned}$$

INTERPRETATION:

- ϵ_{yy} : THE CRYSTAL ELONGATES ALONG THE Y-AXIS BY APPROXIMATELY 0.0004 (OR 0.04%).
- ϵ_{xx} AND ϵ_{zz} : THE CRYSTAL CONTRACTS SLIGHTLY ALONG X AND Z AXES BY APPROXIMATELY 0.0001 (OR 0.01%).

ANALYZING THE RESULTS: MECHANICAL RESPONSE OF THE CRYSTAL

ELASTIC DEFORMATION BEHAVIOR

- THE CRYSTAL RESPONDS ELASTICALLY UNDER

FREQUENTLY ASKED QUESTIONS

WHAT IS THE SIGNIFICANCE OF APPLYING A STRESS OF 92 MPa IN THE $[0\ 1\ 0]$ DIRECTION OF A BCC IRON SINGLE CRYSTAL?

APPLYING A STRESS OF 92 MPa ALONG THE $[0\ 1\ 0]$ DIRECTION HELPS ANALYZE THE MATERIAL'S ELASTIC RESPONSE, YIELD BEHAVIOR, AND THE ONSET OF PLASTIC DEFORMATION SPECIFIC TO THAT CRYSTALLOGRAPHIC ORIENTATION IN BCC IRON.

HOW DO YOU CALCULATE THE RESOLVED SHEAR STRESS ON A SLIP SYSTEM IN BCC IRON WHEN A UNIAXIAL STRESS IS APPLIED?

THE RESOLVED SHEAR STRESS IS CALCULATED USING SCHMID'S LAW: $\tau = \sigma \cos(\phi) \cos(\lambda)$, WHERE σ IS THE APPLIED STRESS, ϕ IS THE ANGLE BETWEEN THE STRESS DIRECTION AND THE SLIP PLANE NORMAL, AND λ IS THE ANGLE BETWEEN THE STRESS DIRECTION AND THE SLIP DIRECTION.

WHAT ARE THE TYPICAL SLIP SYSTEMS IN BCC IRON RELEVANT TO THIS CALCULATION?

THE PRIMARY SLIP SYSTEMS IN BCC IRON ARE $\{1\ 1\ 0\} \langle 1\ 1\ 1 \rangle$. FOR THE $[0\ 1\ 0]$ LOADING DIRECTION, THE SLIP SYSTEMS INVOLVE PLANES AND DIRECTIONS THAT MAXIMIZE RESOLVED SHEAR STRESS, SUCH AS $(1\ 1\ 0) \langle 1\ 1\ 1 \rangle$.

HOW DO YOU DETERMINE THE ANGLES ϕ AND λ FOR THE $[0\ 1\ 0]$ DIRECTION IN BCC IRON'S SLIP SYSTEM?

ANGLES ϕ AND λ ARE DETERMINED BY GEOMETRIC ANALYSIS OF THE CRYSTALLOGRAPHIC ORIENTATION, USING THE DOT PRODUCT BETWEEN THE APPLIED STRESS DIRECTION AND THE SLIP PLANE NORMAL (ϕ), AND BETWEEN THE STRESS DIRECTION AND THE SLIP DIRECTION (λ).

WHAT IS THE CRITICAL RESOLVED SHEAR STRESS (CRSS) FOR SLIP IN BCC IRON, AND HOW DOES IT RELATE TO THE APPLIED 92 MPa STRESS?

THE CRSS IS THE MINIMUM SHEAR STRESS NEEDED TO INITIATE SLIP IN THE CRYSTAL. IF THE RESOLVED SHEAR STRESS FROM THE 92 MPa APPLIED LOAD EXCEEDS THE CRSS, SLIP WILL OCCUR. TYPICAL CRSS FOR BCC IRON IS AROUND 20-30 MPa AT

ROOM TEMPERATURE.

HOW DO TEMPERATURE AND STRAIN RATE INFLUENCE THE CALCULATION OF DEFORMATION UNDER A 92 MPa STRESS IN BCC IRON?

HIGHER TEMPERATURES AND STRAIN RATES CAN INCREASE THE CRSS AND INFLUENCE DISLOCATION MOBILITY, AFFECTING WHETHER THE APPLIED STRESS OF 92 MPa CAN CAUSE PLASTIC DEFORMATION OR ONLY ELASTIC DEFORMATION IN THE CRYSTAL.

CAN YOU DETERMINE WHETHER THE APPLIED STRESS CAUSES ELASTIC OR PLASTIC DEFORMATION IN THE BCC IRON CRYSTAL?

YES, BY CALCULATING THE RESOLVED SHEAR STRESS ON THE PRIMARY SLIP SYSTEM AND COMPARING IT TO THE CRSS, YOU CAN DETERMINE IF THE MATERIAL REMAINS ELASTIC OR UNDERGOES PLASTIC DEFORMATION. IF THE RESOLVED SHEAR STRESS EXCEEDS CRSS, PLASTIC DEFORMATION OCCURS.

WHAT ASSUMPTIONS ARE MADE IN CALCULATING THE STRESS RESPONSE IN A SINGLE CRYSTAL UNDER UNIAXIAL LOAD?

ASSUMPTIONS INCLUDE UNIFORM STRESS DISTRIBUTION, ELASTIC BEHAVIOR WITHIN THE ELASTIC LIMIT, KNOWN CRYSTALLOGRAPHIC ORIENTATION, AND THAT SLIP SYSTEMS OBEY SCHMID'S LAW WITHOUT CONSIDERING DEFECTS OR TEMPERATURE EFFECTS.

HOW DOES THE ORIENTATION OF THE $[0\ 1\ 0]$ DIRECTION INFLUENCE THE CALCULATION OF STRESS AND SLIP ACTIVITY IN BCC IRON?

THE $[0\ 1\ 0]$ ORIENTATION DETERMINES THE ANGLES ϕ AND λ FOR SLIP SYSTEM CALCULATIONS, AFFECTING THE RESOLVED SHEAR STRESS. CERTAIN SLIP SYSTEMS WILL BE MORE FAVORABLY ORIENTED, INFLUENCING THE LIKELIHOOD OF SLIP AND DEFORMATION UNDER THE APPLIED STRESS.

ADDITIONAL RESOURCES

A STRESS OF 92 MPa IS APPLIED IN THE $[0\ 1\ 0]$ DIRECTION OF A UNIT CELL OF A BCC IRON SINGLE CRYSTAL. CALCULATE — THIS SCENARIO PRESENTS A FASCINATING EXPLORATION INTO THE MECHANICS OF CRYSTALLINE MATERIALS, SPECIFICALLY HOW APPLIED STRESSES INFLUENCE THE INTERNAL STATE OF A BODY-CENTERED CUBIC (BCC) IRON CRYSTAL. UNDERSTANDING THE RESPONSE OF SUCH A MATERIAL REQUIRES A DEEP DIVE INTO THE FUNDAMENTAL PRINCIPLES OF CRYSTAL ELASTICITY, THE SYMMETRY OF THE CRYSTAL STRUCTURE, AND THE MATHEMATICAL TOOLS USED TO ANALYZE STRESS AND STRAIN AT THE ATOMIC SCALE.

IN THIS COMPREHENSIVE GUIDE, WE WILL SYSTEMATICALLY DEVELOP THE NECESSARY CONCEPTS TO CALCULATE THE RESULTING STRAIN OR OTHER MECHANICAL RESPONSES WHEN A SPECIFIC STRESS IS APPLIED ALONG A CRYSTALLOGRAPHIC DIRECTION IN A BCC IRON SINGLE CRYSTAL. WHETHER YOU'RE A MATERIALS SCIENTIST, MECHANICAL ENGINEER, OR STUDENT DELVING INTO CRYSTAL MECHANICS, THIS STEP-BY-STEP APPROACH AIMS TO CLARIFY THE PROCESS AND PROVIDE A THOROUGH UNDERSTANDING OF THE UNDERLYING PHYSICS AND MATHEMATICS.

INTRODUCTION TO CRYSTALLINE MATERIALS AND BCC IRON

WHAT IS BCC IRON?

IRON (Fe) EXHIBITS DIFFERENT CRYSTAL STRUCTURES DEPENDING ON TEMPERATURE AND ALLOY COMPOSITION. AT ROOM TEMPERATURE AND STANDARD CONDITIONS, IRON PRIMARILY EXISTS IN THE BODY-CENTERED CUBIC (BCC) STRUCTURE, KNOWN AS ALPHA-IRON OR FERRITE.

- BODY-CENTERED CUBIC (BCC): THE BCC LATTICE CONSISTS OF ATOMS AT THE CORNERS OF A CUBE WITH ONE ATOM IN THE CENTER. IT HAS COORDINATION NUMBER 8 AND A PACKING FACTOR OF APPROXIMATELY 68%.

- SIGNIFICANCE IN MECHANICAL PROPERTIES: BCC IRON HAS RELATIVELY HIGH STRENGTH AND HARDNESS BUT LOWER DUCTILITY COMPARED TO OTHER STRUCTURES LIKE FCC (FACE-CENTERED CUBIC). ITS ELASTIC BEHAVIOR IS ANISOTROPIC, MEANING DIFFERENT CRYSTALLOGRAPHIC DIRECTIONS RESPOND DIFFERENTLY TO APPLIED STRESSES.

CRYSTALLOGRAPHIC DIRECTIONS AND NOTATIONS

- CRYSTALLOGRAPHIC DIRECTIONS ARE EXPRESSED USING MILLER INDICES '[H K L]'. FOR EXAMPLE, '[0 1 0]' INDICATES A DIRECTION ALONG THE Y-AXIS IN THE LATTICE.

- CRYSTALLOGRAPHIC PLANES ARE DENOTED BY '(H K L)'.

IN OUR SCENARIO, THE APPLIED STRESS IS ALIGNED WITH THE '[0 1 0]' DIRECTION, WHICH CORRESPONDS TO A VECTOR ALONG THE Y-AXIS IN THE CRYSTAL LATTICE.

FUNDAMENTALS OF STRESS AND STRAIN IN CRYSTALS

STRESS TENSOR AND ITS SYMMETRY

- STRESS TENSOR (σ): A 3×3 MATRIX REPRESENTING THE INTERNAL FORCES PER UNIT AREA WITHIN A MATERIAL. THE COMPONENTS ARE:

$$\begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix}$$

- PRINCIPAL STRESSES: THE EIGENVALUES OF THE STRESS TENSOR, REPRESENTING MAXIMUM AND MINIMUM NORMAL STRESSES ACTING ON MUTUALLY PERPENDICULAR PLANES.

- APPLIED STRESS IN A DIRECTION: WHEN A UNIAXIAL STRESS IS APPLIED IN A SPECIFIC DIRECTION, IT CAN BE REPRESENTED AS A TENSOR USING THE CONCEPT OF A STRESS VECTOR AND TENSOR TRANSFORMATION.

STRAIN TENSOR AND HOOKE'S LAW IN ANISOTROPIC MATERIALS

- STRAIN TENSOR (ϵ): DESCRIBES THE DEFORMATION STATE OF THE MATERIAL:

$$\begin{bmatrix} \epsilon_{11} & \epsilon_{12} & \epsilon_{13} \\ \epsilon_{21} & \epsilon_{22} & \epsilon_{23} \\ \epsilon_{31} & \epsilon_{32} & \epsilon_{33} \end{bmatrix}$$

- HOOKE'S LAW FOR ANISOTROPIC MATERIALS: RELATES STRESS AND STRAIN VIA THE STIFFNESS TENSOR (C_{ijkl}) OR, EQUIVALENTLY, VIA THE COMPLIANCE TENSOR (S_{ijkl}) :

$$\epsilon_{ij} = S_{ijkl} \sigma_{kl}$$

- IN VOIGT NOTATION, THIS SIMPLIFIES TO:

$$\begin{bmatrix} \boldsymbol{\epsilon} \\ \end{bmatrix} = \mathbf{S} \begin{bmatrix} \boldsymbol{\sigma} \\ \end{bmatrix}$$

WHERE $\begin{pmatrix} \boldsymbol{\epsilon} \end{pmatrix}$ AND $\begin{pmatrix} \boldsymbol{\sigma} \end{pmatrix}$ ARE 6-COMPONENT VECTORS, AND $\begin{pmatrix} \mathbf{S} \end{pmatrix}$ IS THE COMPLIANCE MATRIX.

ELASTIC CONSTANTS OF BCC IRON

THE ELASTIC BEHAVIOR OF BCC IRON CAN BE CHARACTERIZED BY THREE INDEPENDENT ELASTIC CONSTANTS:

- C_{11}
- C_{12}
- C_{44}

VALUES (APPROXIMATE AT ROOM TEMPERATURE):

ELASTIC CONSTANT	VALUE (GPa)
C_{11}	226
C_{12}	138
C_{44}	116

THESE CONSTANTS ENABLE US TO CONSTRUCT THE COMPLIANCE MATRIX AND ANALYZE THE ELASTIC RESPONSE.

STEP-BY-STEP CALCULATION

STEP 1: DEFINE THE APPLIED STRESS

SINCE THE PROBLEM STATES A STRESS OF 92 MPa IS APPLIED IN THE $[0 \ 1 \ 0]$ DIRECTION, THIS INDICATES UNIAXIAL STRESS ALONG THE Y-AXIS.

- STRESS TENSOR FOR UNIAXIAL STRESS IN $[0 \ 1 \ 0]$:

$$\begin{bmatrix} \sigma_{ij} \\ \end{bmatrix} = \sigma \cdot \mathbf{n}_i \mathbf{n}_j$$

WHERE:

- $\sigma = 92 \text{ MPa}$
- $\mathbf{n} = [0, 1, 0]$

THUS, THE STRESS TENSOR:

$$\begin{bmatrix} \sigma_{ij} = 92 \text{ MPa} \cdot \begin{bmatrix} 0 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{bmatrix} \end{bmatrix}$$

IN MATRIX FORM:

```

\l
\SIGMA = \begin{BMATRIX}
0 & 0 & 0 \\
0 & 92\, \text{MPa} & 0 \\
0 & 0 & 0
\end{BMATRIX}
\l

```

STEP 2: CONVERT STRESS TENSOR TO VOIGT NOTATION

VOIGT NOTATION SIMPLIFIES TENSOR COMPONENTS AS:

- $\sigma_1 = \sigma_{11}$
- $\sigma_2 = \sigma_{22}$
- $\sigma_3 = \sigma_{33}$
- $\sigma_4 = \sigma_{23}$
- $\sigma_5 = \sigma_{13}$
- $\sigma_6 = \sigma_{12}$

GIVEN THE STRESS TENSOR:

```

\l
\boldsymbol{\sigma} = \begin{BMATRIX}
0 \\
92\, \text{MPa} \\
0 \\
0 \\
0 \\
0
\end{BMATRIX}
\l

```

STEP 3: CONSTRUCT THE COMPLIANCE MATRIX $\mathbf{S}$

USING THE ELASTIC CONSTANTS FOR BCC IRON:

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\l
\mathbf{S} = \begin{BMATRIX}
\frac{1}{C_{11}} + \frac{1}{C_{12}} & -\frac{C_{12}}{C_{11} C_{12}} & -\frac{C_{12}}{C_{11} C_{12}} & 0 & 0 & 0 \\
-\frac{C_{12}}{C_{11} C_{12}} & \frac{1}{C_{11}} + \frac{1}{C_{12}} & -\frac{C_{12}}{C_{11} C_{12}} & 0 & 0 & 0 \\
-\frac{C_{12}}{C_{11} C_{12}} & -\frac{C_{12}}{C_{11} C_{12}} & \frac{1}{C_{11}} + \frac{1}{C_{12}} & 0 & 0 & 0 \\
\frac{1}{C_{12}} & \frac{1}{C_{12}} & \frac{1}{C_{12}} & \frac{1}{C_{44}} & 0 & 0 \\
0 & 0 & 0 & 0 & \frac{1}{C_{44}} & 0 \\
0 & 0 & 0 & 0 & 0 & \frac{1}{C_{44}}
\end{BMATRIX}
\l

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BUT IT'S MORE STRAIGHTFORWARD TO USE THE STANDARD FORM:

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\l
\mathbf{S} = \begin{BMATRIX}
\frac{1}{C_{11} + C_{12}} & -\frac{C_{12}}{(C_{11} + C_{12}) C_{12}} & -\frac{C_{12}}{(C_{11} + C_{12}) C_{12}} & 0 & 0 & 0 \\
-\frac{C_{12}}{(C_{11} + C_{12}) C_{12}} & \frac{1}{C_{11}} & -\frac{C_{12}}{C_{11} C_{12}} & 0 & 0 & 0 \\
-\frac{C_{12}}{(C_{11} + C_{12}) C_{12}} & -\frac{C_{12}}{C_{11} C_{12}} & \frac{1}{C_{11}} & 0 & 0 & 0 \\
0 & 0 & 0 & \frac{1}{C_{44}} & 0 & 0 \\
0 & 0 & 0 & 0 & \frac{1}{C_{44}} & 0 \\
0 & 0 & 0 & 0 & 0 & \frac{1}{C_{44}}
\end{BMATRIX}
\l

```

$\frac{0}{0}$

A Stress Of 92 Mpa Is Applied In The 0 0 1 Direction Of A Unit Cell Of A Bcc Iron Single Crystal Calculate

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